# Preparation of a Novel Copper Catalyst in Terms of the Immiscible Interaction Between Copper and Chromium

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**Abstract** Based on the metallurgical point of view, we aimed to design a new form of copper catalysts with high thermal stability and activity. Delafossite CuCrO<sub>2</sub> has been studied as a precursor for copper catalyst. The CuCrO<sub>2</sub> was reduced to fine dispersion of Cu and Cr<sub>2</sub>O<sub>3</sub> particles with porous structure by the treatment in H<sub>2</sub> at 600 °C, which exhibited much higher activity and thermal stability for steam reforming of methanol (SRM) than those of the CuO and/or Cr<sub>2</sub>O<sub>3</sub> catalysts. Sintering of Cu particles was significantly suppressed even after H<sub>2</sub> reduction at 600 °C. Moreover, the CuCrO<sub>2</sub> can be regenerated by calcination in air at 1,000 °C where the activity is also restored completely even after sintering at high temperatures. Fine porous structure generated by the reduction of CuCrO2 and immiscible interaction between Cu and Cr<sub>2</sub>O<sub>3</sub> are important in stabilizing of copper nanoparticles. Based on these findings, we propose that the CuCrO<sub>2</sub> is an effective precursor for a high performance copper catalyst.

**Keywords**  $CuCrO_2 \cdot Delafossite \cdot Immiscible \cdot Porous structure \cdot Thermal stability \cdot Reversible \cdot Methanol steam reforming$ 

#### 1 Introduction

Copper-based catalysts are extensively studied due to their good catalytic performance in several reactions such

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as steam reforming of methanol and water gas shift reaction [1, 2]. Difficulty of homogeneous dispersion of Cu particles on supports and poor thermal stability have been the major drawbacks [3]. To overcome these problems, catalytic performance of copper-based catalysts has been improved by combination with the metal oxides such as ZnO [3-5], Cr<sub>2</sub>O<sub>3</sub> [5, 6], Fe<sub>2</sub>O<sub>3</sub> [7, 8], and CoO [9]. However, roles of the oxides in the improved copperbased catalysts have not been sufficiently understood. According to the binary alloy equilibrium phase diagrams, Cu and M (M = Fe, Cr, Co, etc.) are neither form compounds nor mutually dissolve in the solid state, i.e., Cu and M are immiscible [10]. Recently, we have found that copper catalysts with fine dispersion of copper particles and high thermal stability can be directly prepared from a spinel CuFe<sub>2</sub>O<sub>4</sub> in which the combination of Cu with Fe is important [7, 11]. High catalytic performance is ascribed to the reduction of the spinel CuFe<sub>2</sub>O<sub>4</sub> and the subsequent immiscible interaction between Cu and Fe [7]. The origin of high catalytic performance is due to the formation of a composite structure induced by reductive decomposition of the CuFe<sub>2</sub>O<sub>4</sub> where nano-scale copper particles homogenously dispersed within the porous Fe<sub>3</sub>O<sub>4</sub> matrix [11]. With understanding of interaction between the constituent metals in mixed oxides, one may logically design a promising catalyst. In this material design, metallurgical background is very helpful.

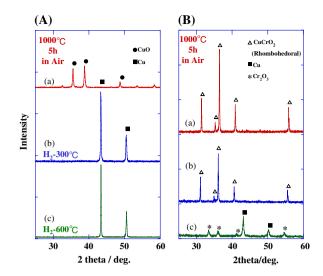
Based on the metallurgical point of view, we have investigated a process for preparation of a new form of copper catalysts with high catalytic performance. In this work, we examine the morphological change before and after reduction and the regeneration of the delaffosite CuCrO<sub>2</sub> in the redox treatments and claim the role of the interaction of chromium (or chromium oxides) with copper in the CuCrO<sub>2</sub>.

## 2 Experimental

The CuCrO<sub>2</sub> catalyst was prepared by the following method. Stoichiometric mixtures (atomic ratio Cu/Cr = 1) of high purity CuO (NanoTek, C.I. Kasei Co.) and Cr<sub>2</sub>O<sub>3</sub> (Wako Pure Chemical Industries, Ltd.) powders were homogenized in an agate mortar. The mixed powder was calcined in air at 1,000 °C for 12 h and cooled down slowly. For comparison, CuO and CuO + Cr<sub>2</sub>O<sub>3</sub> (physical mixture) catalyst were also studied. The steam reforming of methanol (SRM) experiments were carried out in a conventional flow reactor at 100 kPa. Inlet partial pressure of methanol, water and nitrogen were 35.5, 52.7, and 13.2 kPa, respectively (LHSV of CH<sub>3</sub>OH/H<sub>2</sub>O mixture: 30 h<sup>-1</sup>). Here nitrogen was used as dilutent. All samples were pretreated with H<sub>2</sub> at 460 or 600 °C for 1 h in a flow reactor before reaction. The products were analyzed by an on-line gas chromatograph (Shimadzu GC 14A) equipped with Shincarbon column (H<sub>2</sub>, CO, CO<sub>2</sub>, and CH<sub>4</sub>) under Ar carrier gas. The catalytic activity for the SRM was evaluated by the H<sub>2</sub> production rate (mL STP min<sup>-1</sup> g-cat<sup>-1</sup>). The data in the catalytic activity measurements were recorded when the reaction reached steady state after 30 min. The turnover frequencies (TOFs) were calculated by dividing the H<sub>2</sub> production rate by the total amount of surface copper atoms. The total amount of the surface copper metal sites was estimated by oxygen adsorption on reduced Cu via N2O decomposition at 90 °C:  $N_2O + 2Cu_s^0 \rightarrow Cu_2O + N_2 \uparrow$ where Cu<sub>s</sub> is a surface Cu atom [12]. Surface area determination of particle was made by BET analysis. Pore structure and pore size distributions of the samples were obtained from N<sub>2</sub> adsorption-desorption isotherms at -196 °C. The phase identification of each sample was performed by X-ray diffraction (Mac science M03XHF22) using Cu K $\alpha$  ( $\lambda$  = 1.543 Å) radiation. The copper crystallite sizes of the samples were estimated from the XRD line broadening analysis using the Scherrer equation for the Cu(111) reflection. The H<sub>2</sub>-TPR measurements were carried out using 50 mg of the catalyst from room temperature to 600 °C at a heating rate of 4 °C/min in 5% H<sub>2</sub>/Ar flow (30 mL/min). The surfaces of the samples were observed by a scanning electron microscopy (LEO 982).

## 3 Results and Discussion

Figure 1 shows the XRD patterns of  $CuCrO_2$  catalyst before and after  $H_2$  reduction treatment. As shown in Fig. 1, the peaks responsible for delafossite  $CuCrO_2$  were observed before  $H_2$  reduction [13]. It is noted that a single phase of the delafossite  $CuCrO_2$  was formed in the mixture of CuO and  $Cr_2O_3$  calcinated in air at 1,000 °C [13, 14]. Figure 2 shows the  $H_2$ -TPR profile of the  $CuCrO_2$  catalyst.



**Fig. 1** Powder X-ray diffraction patterns of the CuO (**A**) and the CuCrO<sub>2</sub> (**B**) as a function of  $H_2$  reduction temperature: (**a**) before, (**b**) 460 °C, and (**c**) 600 °C

As shown in Fig. 2, a peak responsible for reduction around 670 °C is observed for the  $CuCrO_2$  catalyst, which is attributed to the reduction of  $CuCrO_2$  to Cu and  $Cr_2O_3$ . The changes in XRD patterns along the reduction temperature are in good consistent with the TPR profile for the  $CuCrO_2$  catalyst. The XRD patterns and the  $H_2$ -TPR profile of CuO are also shown in Figs. 1 and 2 for comparison. As shown in Fig. 1, after the  $H_2$  reduction, the diffraction peaks of Cu are very sharp when the precursor is CuO, while those are much broadening when the precursor is  $CuCrO_2$ , indicating that sintering of Cu particles generated from the  $CuCrO_2$  has been significantly suppressed by the presence of chromium even after the  $H_2$  reduction at high temperatures ( $\sim 600$  °C).

Table 1 summarized the results of the BET surface area measurement. It is clear that the surface area of the CuCrO<sub>2</sub> increases by one order after H<sub>2</sub> reduction at 600 °C. In contrast, the surface areas of the CuO and the CuO + Cr<sub>2</sub>O<sub>3</sub> catalysts drastically decrease after the H<sub>2</sub> reduction treatments. Figure 3 shows the pore size distribution estimated from the BET measurement before and after H<sub>2</sub> reduction for the CuCrO2. After H2 reduction at 600 °C, the CuCrO<sub>2</sub> catalyst showed the broad pore size distribution with a peak around 7 nm, indicating that the observed increase in surface area is due to formation of these fine meso-pores. For the CuO and the CuO + Cr<sub>2</sub>O<sub>3</sub> catalysts after H<sub>2</sub> reduction, the surface areas are smaller than  $0.05 \text{ m}^2/\text{g}$  for the CuO and  $1.1 \text{ m}^2/\text{g}$  for the CuO + Cr<sub>2</sub>O<sub>3</sub>, respectively, which are much smaller than that of the Cu-CrO<sub>2</sub> catalyst. This is ascribed to the fact that the copper particles readily aggregate during H2 reduction at high temperatures. Figure 4 shows the SEM micrographs of the CuCrO<sub>2</sub> catalyst before and after H<sub>2</sub> reduction treatments.



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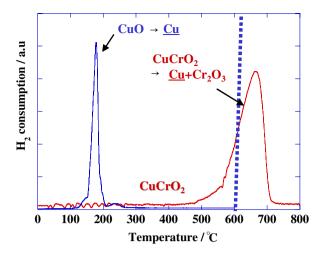


Fig. 2  $H_2$ -TPR profiles of the CuO and the CuCrO<sub>2</sub> powders. TPR conditions: heating at 4 °C/min in 5%  $H_2$ /Ar

The CuCrO $_2$  surface was smooth before  $H_2$  reduction, whereas precipitates came up on the surface after  $H_2$  reduction at 460 °C. The precipitates are attributed to composite products, i.e.,  $Cu + Cr_2O_3$ , by reductive decomposition of outmost surface of  $CuCrO_2$  bulk. After  $H_2$  reduction at 600 °C, the  $CuCrO_2$  completely decomposed to copper and chromium oxide as verified by the XRD measurement. It should be noted that the  $Cr_2O_3$  reveals very fine porosity, which is responsible to the high surface area and mesopore obtained by BET measurements. This indicates that the formation of mesopore was achieved by reductive decomposition of the  $CuCrO_2$ .

Figure 5 shows the rate of  $H_2$  production as a function of reaction temperature in the SRM over the  $CuCrO_2$ , the CuO and the  $CuO + Cr_2O_3$  catalysts after  $H_2$  reduction at 600 °C. The  $CuCrO_2$  catalyst significantly exhibited much higher catalytic activity than the CuO and the  $CuO + Cr_2O_3$  catalysts. The catalytic activity of the  $CuCrO_2$  catalyst treated at 460 °C in  $H_2$  was very low due to insufficient reduction for the  $CuCrO_2$  (not shown). As

**Table 1** Results of BET surface area measurements  $(m^2/g)$ , crystallite sizes (nm), and TOF values  $(s^{-1})$ 

Catalyst	Before <sup>a</sup> (m <sup>2</sup> /g)	After H <sub>2</sub> reduction <sup>b</sup> (m <sup>2</sup> /g)	Crystallite size <sup>c</sup> (nm)	TOF <sup>d</sup> (10 <sup>-1</sup> s <sup>-1</sup> )
CuO	10.8	< 0.05	56	0.1
CuO + Cr2O3 $(Cu/Cr = 1)$	7.0	1.1	29	2.0
CuCrO <sub>2</sub>	0.2	2.7	17	26.0

<sup>&</sup>lt;sup>a</sup> Before H<sub>2</sub> reduction

<sup>&</sup>lt;sup>d</sup> Reaction temperature at 280 °C



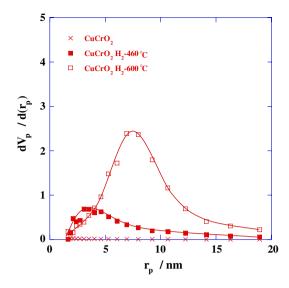


Fig. 3 Pore distribution in the CuCrO<sub>2</sub> powders before and after  $H_2$  reduction: (×) before, ( $\blacksquare$ ) at 460 °C, and ( $\square$ ) at 600 °C

shown in Table 1, the TOF value of the  $CuCrO_2$  catalyst is more than 30 and 10 times higher than those of the CuO and the  $CuO + Cr_2O_3$  catalysts, respectively. Decrease of surface area and sharpening of diffraction peaks of copper in the CuO and the  $CuO + Cr_2O_3$  catalysts were observed after  $H_2$  reduction at 600 °C, indicating that sintering of copper particles readily proceed during reduction. On the other hand, the copper particles generated from the  $CuCrO_2$  showed high catalytic activity and thermal stability. The fine porous structure forms by  $H_2$  reduction of the  $CuCrO_2$ , which leads to the increase in the effective surface area of copper responsible for catalytic reaction.

For comparison, it is of interesting to examine reduction behavior and catalytic activity of spinel  $CuCr_2O_4$  as a copper chromite related compound. Although the  $CuCr_2O_4$  was not active for the SRM reaction (without  $H_2$  reduction treatment), the catalytic activity of the  $CuCr_2O_4$  exhibited almost comparable activity to the  $CuCr_2O_4$  after the  $H_2$  reduction at 600 °C for 1h (not shown). The reduction of the  $CuCr_2O_4$  during the  $H_2$  treatment proceeds as follows:  $CuCr_2O_4 \rightarrow (CuCrO_2 + Cu + Cr_2O_3) \rightarrow Cu + Cr_2O_3$ , which have been reported by several research groups [15–17]. This is suggested that reduction of both the  $CuCr_2O_4$  and the  $CuCrO_2$  leads to form similar composite phases  $(Cu + Cr_2O_3)$  after the  $H_2$  pretreatment at 600 °C.

In this study, we have shown a copper catalyst with high thermal stability and revealing high catalytic activity developed from the  $CuCrO_2$ . The origin of high activity and high thermal stability is the formation of a porosity structure generated by reduction of the  $CuCrO_2$  where nano-scale Cu particles homogenously dispersed within the porous  $Cr_2O_3$  (i.e., fine dispersion of copper particles). Remarkable increase in surface area after  $H_2$  reduction at 600 °C is clearly derived from the formation of the porous

<sup>&</sup>lt;sup>b</sup> After H<sub>2</sub> reduction at 600 °C for 1 h

 $<sup>^</sup>c$  Calculated from the XRD patterns after  $H_2$  reduction at 600  $^o\text{C}$  using the Scherrer equation for the Cu(111) reflection

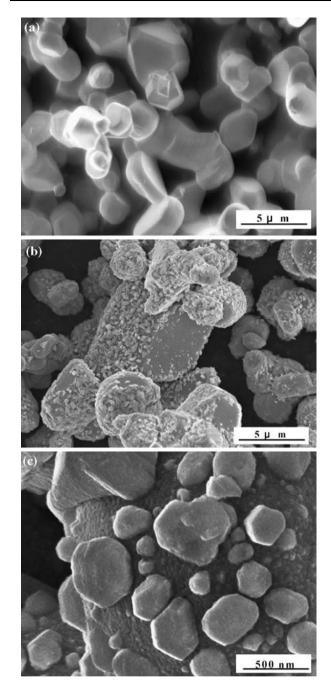


Fig. 4 SEM images for the CuCrO<sub>2</sub>: (a) before and after  $H_2$  reduction treatment, (b) at 460 °C, and (c) at 600 °C

structure. Undoubtedly, the high catalytic activity is attributed to the spontaneous formation of fine copper particles dispersed in the porous chromium oxide. On the other hand, it is known in phase diagram that Cu and Cr are mutually immiscible [10], and the phase separation between copper and chromium oxide at nano-scale could keep high dispersion and high thermal stability of Cu particles.

In the  $H_2$ -TPR and the XRD measurements, it is clear that the  $CuCrO_2$  is reduced to  $Cu^*$  (fine dispersion of

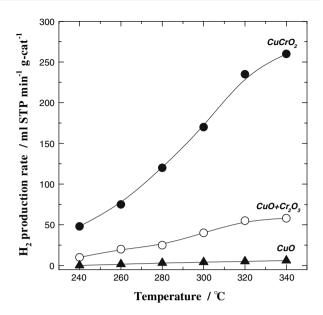


Fig. 5 The rate of  $H_2$  production versus reaction temperatures in the steam reforming of methanol for the CuO, the (CuO +  $Cr_2O_3$ ) and the CuCrO<sub>2</sub> powders after  $H_2$  reduction at 600 °C

copper nanoparticles) and  $Cr_2O_3$  particles around 600 °C (Eq. (1)). Fine dispersion of copper nanoparticles is attainable by the  $H_2$  reduction of the  $CuCrO_2$ . These properties are ascribed to the selective reduction of the  $CuCrO_2$  and the subsequent immiscible interaction between copper and chromium (or chromium oxides). Interestingly, the  $CuCrO_2$  can be regenerated by treatment in air at 1,000 °C even if an intentional sintering of copper particles occurs (i.e., reversible process).

$$CuCrO_2 \leftrightarrow Cu^* + Cr_2O_3 \tag{1}$$

In general, due to the immiscibility of copper with chromium nanostructure with Cu and Cr cannot be obtained by conventional alloying processes such as arc melting [10]. However, Cu and Cr atoms distribute homogenously at atomic scale in a composite oxide. Composite oxides in this case act as precursors in which Cu nanoparticles are readily formed by the  $H_2$  reduction. In this study, we propose a simple process to design a new copper catalyst based on the concept described above. Change in the morphology of the  $CuCrO_2$  under the redox condition deserves further attention to expand into more detailed studies including the formation of the porous structure from the  $CuCrO_2$  and its mechanism.

## 4 Conclusions

The present study demonstrates the validity of delafossite CuCrO<sub>2</sub> as a precursor for a high catalytic performance copper catalyst. The structure consisting of fine dispersion



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of Cu particles within the porous chromium oxides was obtained by the  $\rm H_2$  reduction at 600 °C for the CuCrO<sub>2</sub>, reveals high surface area and catalytic activity for SRM. The high thermal stability is ascribed to the formation of the porous structure and the subsequent immiscible interaction between Cu and  $\rm Cr_2O_3$ . Additionally, the delafossite CuCrO<sub>2</sub> was readily regenerated by calcination in air at 1.000 °C.

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