

## Incorporation of $\text{La}^{3+}$ into a $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$ catalyst

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The effects of  $\text{La}^{3+}$  incorporation into a  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst were investigated by a combination of activity, temperature-programmed reduction (TPR), oxygen storage capacity (OSC), noble-metal surface area, and X-ray diffraction (XRD) measurements. Incorporation of  $\text{La}^{3+}$  ions into the  $\text{Al}_2\text{O}_3$ , before  $\text{CeO}_2$  is added, promoted higher Pt and  $\text{CeO}_2$  dispersions. The oxygen storage capacity was also higher in the presence of  $\text{La}^{3+}$ . This is attributed to a combination of Pt and  $\text{CeO}_2$  particle-size effects and possible blockage of the reaction between  $\text{Al}_2\text{O}_3$  and  $\text{CeO}_2$ . The XRD data show that  $\text{La}^{3+}$  forms  $\text{LaAlO}_3$  with  $\text{Al}_2\text{O}_3$  and prevents  $\alpha$ - $\text{Al}_2\text{O}_3$  formation after various heat treatments.

**Keywords:** lanthana; alumina; ceria; Pt; three-way catalyst; oxygen storage; X-ray diffraction; CO chemisorption; temperature-programmed reduction

### 1. Introduction

The present-day automotive three-way catalyst (TWC) contains a number of ingredients, each typically intended to perform a particular function. Lanthana ( $\text{La}_2\text{O}_3$ ), for example, known to be one of the most effective inhibitors of alumina surface area loss [1], has long been added at levels required to optimally achieve just this result. But the addition of  $\text{La}_2\text{O}_3$  has also been linked to other effects such as increased rich-side  $\text{NO}_x$  conversion in Pd-based catalysts [2] and higher noble-metal dispersion [3]. Recent observations [4] suggest that  $\text{La}_2\text{O}_3$  may further promote more efficient utilization of yet another ingredient of the TWC, ceria ( $\text{CeO}_2$ ), which serves primarily as an oxygen storage component [5–12]. Specifically,  $\text{La}^{3+}$ -modified alumina-supported ceria was found to display a smaller intrinsic  $\text{Ce}^{3+}$  fraction, a larger  $\text{CeO}_2$  dispersion, and a greater range of reversible reducibility than in the unmodified case. The present study, incorporating Pt as a catalytically active ingredient, was undertaken to determine whether these changes translate into observable effects in an actual catalyst.

## 2. Experimental

### 2.1. CATALYST PREPARATION

Samples of 10 wt% La<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and 10 wt% CeO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalysts were prepared by impregnating γ-Al<sub>2</sub>O<sub>3</sub> washcoated ceramic cordierite with La(NO<sub>3</sub>)<sub>3</sub>·5H<sub>2</sub>O and Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O solutions of the desired concentration by the incipient wetness method. The samples were dried at 373 K and calcined at 773 K for 5 h. The 10 wt% CeO<sub>2</sub>/10 wt% La<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> sample was prepared by impregnating the calcined 10 wt% La<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> sample with Ce(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O solution of the desired concentration. This sample was again dried at 373 K and calcined at 773 K for 5 h.

Catalysts containing 0.6 wt% Pt were then prepared by stepwise impregnation of 10 wt% CeO<sub>2</sub>/10 wt% La<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and 10 wt% CeO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> with H<sub>2</sub>PtCl<sub>6</sub> solution. The catalysts were dried at 373 K and calcined at 773 K for 5 h. Unless otherwise noted, the 0.6 wt% Pt/10 wt% CeO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalyst is referred to as Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> and the 0.6 wt% Pt/10 wt% CeO<sub>2</sub>/10 wt% La<sub>2</sub>O<sub>3</sub>/γ-Al<sub>2</sub>O<sub>3</sub> catalyst as Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub>.

### 2.2. CATALYST PRETREATMENT

The catalysts prepared by the methods outlined above are referred to as “fresh” catalysts in this report. Samples of the fresh catalysts were subjected to one of two pretreatments to study various aging effects. Thermally treated samples were subjected to dynamic aging by treatment at 1073 K for 4 h under simulated exhaust gas oscillating between lean and rich compositions at a frequency of 0.05 Hz. A detailed description of the laboratory reactor system has been reported recently [13]. The feed gas composition was 1500 vol. ppm HC (consisting of 1000 vol. ppm C<sub>3</sub>H<sub>6</sub> and 500 vol. ppm C<sub>3</sub>H<sub>8</sub>), 1.3% CO, 0.33% H<sub>2</sub>, 20 vol. ppm SO<sub>2</sub>, and 974 vol. ppm NO. For the dynamic aging, the O<sub>2</sub> concentration was adjusted to vary the redox ratio between 0.89 (lean) and 1.16 (rich), and the N<sub>2</sub> concentration in the primary feed was adjusted accordingly to keep the space velocity constant. In addition to the dynamic aging, some of the samples were hydrothermally treated by aging in 10% H<sub>2</sub>O in flowing air (200 cm<sup>3</sup>/min) at 1223 K for 24 h.

### 2.3. ACTIVITY

Catalyst activity was measured using the same reactor setup as for thermal aging but without cycling the gas composition. Two types of experiments were performed, both at 60 000 h<sup>-1</sup> space velocity. In the first, the catalyst temperature was increased stepwise from room temperature and the temperatures required for 50% conversion of each species (referred to as light-off temperatures) were

recorded. In the second type of experiment, conversions of CO, NO<sub>x</sub>, and HC were measured at 823 K as a function of the molar ratio of reducing species to oxidizing species,  $R$ , varied by changing the amount of O<sub>2</sub> in the feed while holding the other concentrations constant ( $R < 1$  = excess oxidants;  $R = 1$  stoichiometric;  $R > 1$  excess reductants).

#### 2.4. TEMPERATURE-PROGRAMMED REDUCTION

TPR experiments were carried out on an Altamira temperature programmed system. The details of the TPR apparatus have been reported elsewhere [14]. Oxidizing pretreatments were carried out in the TPR cell in a 40 cm<sup>3</sup>/min flow of 10% O<sub>2</sub> in He at 823 K for 50 min. The samples were cooled in O<sub>2</sub> to 277 K before the start of the temperature programmed reduction. The samples were heated in 9% H<sub>2</sub> in Ar to 873 K at a rate of 30 K/min and the H<sub>2</sub> consumption was monitored with a thermal conductivity detector.

#### 2.5. OXYGEN STORAGE CAPACITY

The oxygen storage capacity measurements were conducted using a 3.62 cm<sup>3</sup> sample of the fresh and thermally aged catalysts. A thermocouple imbedded into the monolithic sample was used to monitor the temperature, while a network of solenoid valves enabled the injection of alternating pulses of carbon monoxide (1% in helium) and oxygen (0.5% in helium) at an overall flow rate of 3000 cm<sup>3</sup>/min. Switching between gases was performed simultaneously at a frequency of 0.016 Hz, and gas sampling was accomplished through a sapphire leak valve into a quadrupole mass spectrometer using one stage of differential pumping. Oxygen storage capacity was computed from the rate of carbon monoxide removal immediately following the transition from oxygen to carbon monoxide with the sample at a temperature of 873 K.

#### 2.6. NOBLE-METAL SURFACE AREA

A CO–H<sub>2</sub> titration method (i.e. methanation) [15] was used to determine Pt surface area on the Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> and Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> catalysts. A small amount (approximately 0.1 g) of each sample was ground and packed in a glass U-tube in a “sandwich” of quartz wool. Each sample was oxidized in flowing O<sub>2</sub> (40 cm<sup>3</sup>/min) for 30 min at 673 K and then reduced at 673 K in flowing H<sub>2</sub> (40 cm<sup>3</sup>/min) for 30 min. After cooling the sample to room temperature in flowing H<sub>2</sub>, two CO pulses of 2 cm<sup>3</sup> each were introduced to the sample with H<sub>2</sub> as a carrier gas. The sample was purged with H<sub>2</sub> for 10 min. The reactor tube was then sealed by closing three-way valves to trap the H<sub>2</sub> and the adsorbed CO. The sample was heated at 673 K for 30–45 min to hydrogenate the adsorbed CO. The amount of CH<sub>4</sub> formed after the reaction was measured by a flame ionization detector on a Varian Star 3400 gas chromatograph.

## 2.7. X-RAY DIFFRACTION (XRD)

XRD measurements were performed on the fresh and hydrothermally aged Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> and Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> samples in order to determine the phases and Pt and CeO<sub>2</sub> particle sizes. XRD patterns were recorded on a Philips X-ray generator with a Debye-Scherrer camera. Cu K $\alpha$  X-rays ( $\lambda = 1.5418 \text{ \AA}$ ) were used as the X-ray source. The XRD apparatus used to analyze the samples has been described in detail previously [14].

## 3. Results

### 3.1. ACTIVITY

Light-off temperatures for fresh and thermally aged samples of both catalysts were found to be just below 773 K. This is relatively high compared to a fully formulated TWC which usually contains Rh in addition to either Pt or Pd, but is not unexpected for such a Pt-only catalyst. The  $R$  curves generated at a temperature of 823 K from the fresh catalysts are shown in figs. 1 and 2. The main differences are higher NO<sub>x</sub> and CO conversions and lower HC conversion for the Pt/CeO<sub>2</sub>/

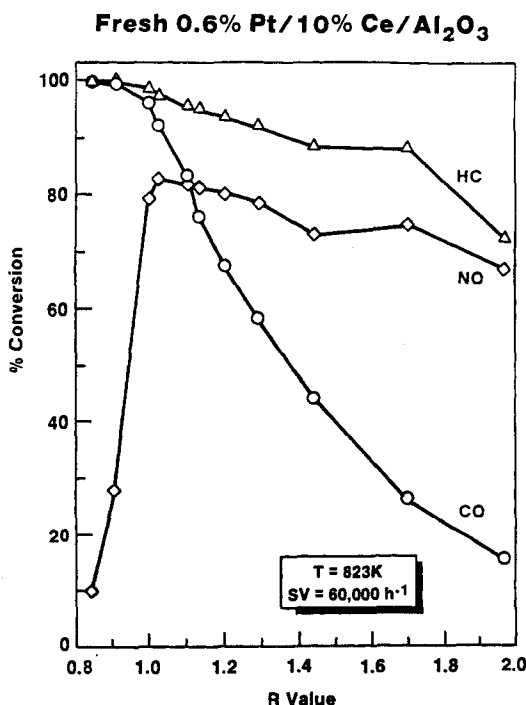


Fig. 1. Conversion efficiency of the fresh Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst as a function of  $R$ , the molar ratio of reducing to oxidizing species in the feed gas.

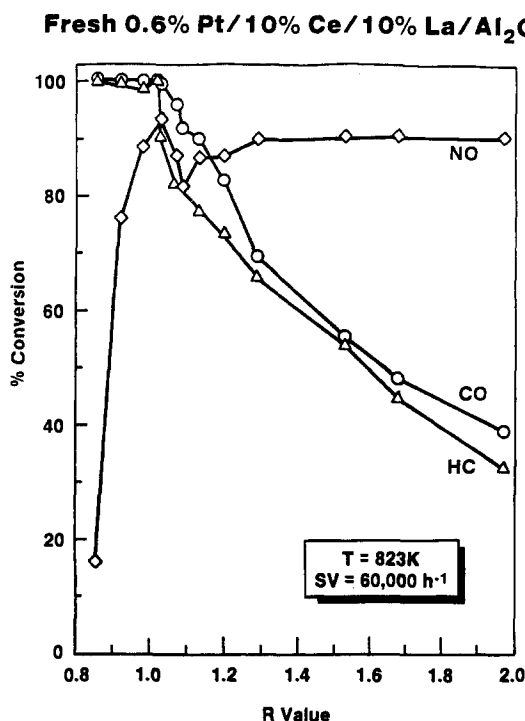


Fig. 2. Conversion efficiency of the fresh  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst as a function of  $R$ , the molar ratio of reducing to oxidizing species in the feed gas.

$\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst. In addition, for the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst, the overall conversion of CO and HC on the rich side exceeds somewhat the  $\text{O}_2$  and NO available, implying that water-gas shift or steam reforming reactions may be more important for this catalyst.

### 3.2. TEMPERATURE-PROGRAMMED REDUCTION

The reduction profiles for the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  and  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalysts after various thermal treatments are presented in figs. 3 and 4, respectively. Table 1 summarizes the  $\text{H}_2$  consumed during reduction of these catalysts, obtained by integrating the area under the TPR traces, and compares it to the theoretical  $\text{H}_2$  consumption.

The following trends were observed after either thermal aging in the reactor or hydrothermal aging of the fresh  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst: (1) the broad low temperature peak (below 450 K) and the sharp peak at 515 K decreased sharply after thermal aging; these peaks were absent in the hydrothermally aged sample, (2) the broad peak around 740 K increased in size and shifted to lower temperature after thermal aging; it was absent in the hydrothermally aged sample, (3) the broad, high temperature peak extending from 800 to about 1150 K increased sharply in magni-

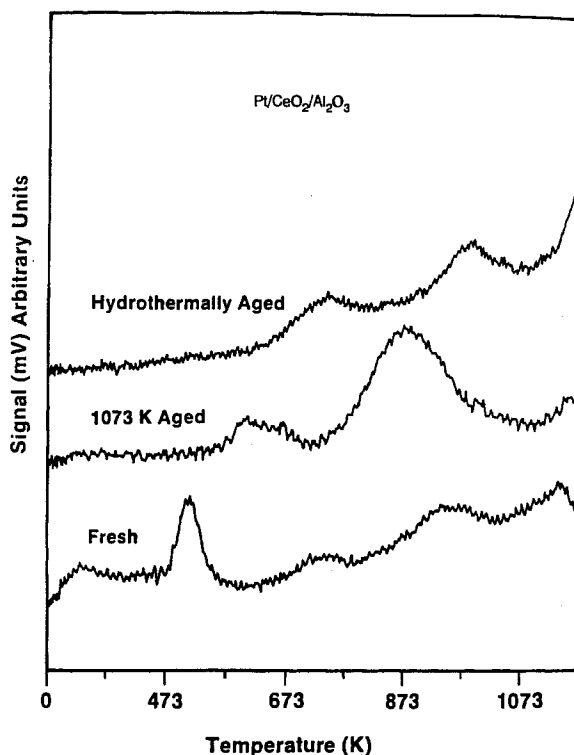


Fig. 3. TPR spectra of the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst after various treatments.

tude and shifted to lower temperature after thermal aging; the peak intensity decreased sharply and the maximum shifted further down to lower temperature and a new broad peak appeared at 1000 K after hydrothermal aging. Pretreatments of the  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst produced similar trends to those observed with the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst.

The total amount of  $\text{H}_2$  consumed during the reduction of the fresh  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst decreased sharply from 260 to 111  $\mu\text{mol/g}$  (31.5% of the theoretical  $\text{H}_2$  consumption) upon thermal aging. Hydrothermal aging of this catalyst proved to be harsh also, the total  $\text{H}_2$  consumption decreasing to 131  $\mu\text{mol/g}$  (37% of the theoretical  $\text{H}_2$  consumption). In the case of the  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst, the total amount of  $\text{H}_2$  consumed decreased from 260  $\mu\text{mol/g}$  for the fresh catalyst to 194  $\mu\text{mol/g}$  (55% of the theoretical  $\text{H}_2$  consumption) for the thermally aged catalyst. The  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst thus retains more reducible oxides than the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst (55% of the theoretical  $\text{H}_2$  consumption in the  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst as compared to only 31.5% in the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst) after thermal aging. After hydrothermal aging, however, the total amount of  $\text{H}_2$  consumption again decreased to 131  $\mu\text{mol/g}$  (37% of the theoretical  $\text{H}_2$  consumption), identical to the decrease observed for the  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst.

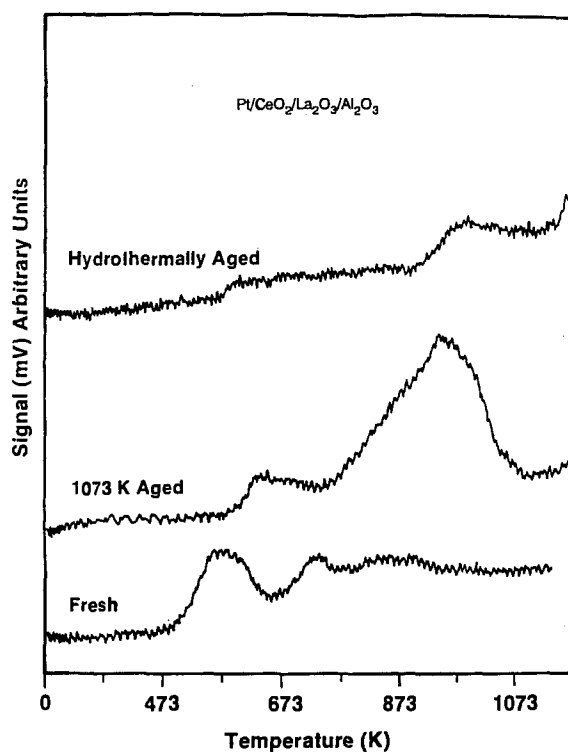
Fig. 4. TPR spectra of the  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst after various treatments.

Table 1

Sample	H <sub>2</sub> consumption <sup>a</sup> (μmol/g)	OSC <sup>b</sup> (μmol-O/g s)	Dispersion (%)	XRD particle size (nm)	
				Pt	CeO <sub>2</sub>
<i>fresh</i>					
Pt/CeO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	260	4.4	20.7	<7	8 ± 2
Pt/CeO <sub>2</sub> /La <sub>2</sub> O <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub>	260	9.1	24.9	<7	4 ± 2
<i>thermally aged</i>					
Pt/CeO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	111	2.4	0.5	—	—
Pt/CeO <sub>2</sub> /La <sub>2</sub> O <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub>	194	5.7	4.5	—	—
<i>hydrothermally aged</i>					
Pt/CeO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	131	—	0.65	160 ± 30	20 ± 2
Pt/CeO <sub>2</sub> /La <sub>2</sub> O <sub>3</sub> /Al <sub>2</sub> O <sub>3</sub>	131	—	1.35	100 ± 30	13 ± 2

<sup>a</sup> Theoretical  $\text{H}_2$  consumption is  $352 \mu\text{mol/g}$  for all samples, assuming  $\text{PtO}_2 \rightarrow \text{Pt}$  and  $\text{CeO}_2 \rightarrow \text{Ce}_2\text{O}_3$ .

<sup>b</sup> OSC: oxygen storage capacity.

### 3.3. OXYGEN STORAGE CAPACITY

Oxygen storage capacities are listed in table 1, where it can be seen that the Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst has about twice the capacity of the Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst, both in the fresh and thermally aged states.

### 3.4. NOBLE-METAL SURFACE AREA

Dispersion measurements for each sample are presented in table 1. The dispersion measurements were carried out after the pretreatments described in the experimental section. The estimated noble metal dispersions are based on the assumed ratio of Pt<sub>surface atoms</sub> : CO<sub>adsorbed</sub> : CH<sub>4</sub><sub>formed</sub> = 1. Previous studies [15] have shown that the assumed ratio of one methane molecule formed per CO molecule adsorbed is accurate.

The percentage dispersion was higher for the fresh Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst than for the fresh Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst (24.9 and 20.7%, respectively). In all cases, the percentage dispersion dropped dramatically after aging. However, the samples with La<sup>3+</sup> yielded higher Pt dispersions than the samples without La<sup>3+</sup> (4.5% versus 0.5% after thermal aging and 1.35% versus 0.65% after hydrothermal aging).

### 3.5. X-RAY DIFFRACTION

Diffraction patterns from both fresh and hydrothermally aged samples of the two catalysts are shown in figs. 5 and 6, where differences in phase composition and Pt and CeO<sub>2</sub> particle size are apparent. In particular,  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> is present in the Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> sample while LaAlO<sub>3</sub> is present in the Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> sample after hydrothermal aging, and the Pt and CeO<sub>2</sub> particles are always smaller in the sample containing La<sup>3+</sup>. Estimates of the latter, derived from line broadening, are listed in table 1.

## 4. Discussion

As the noble-metal surface area and XRD measurements show, the addition of La<sup>3+</sup> to the Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst has the effect of increasing both Pt and CeO<sub>2</sub> dispersions. A similar effect of La<sup>3+</sup> on Rh dispersion, qualitatively like that of Ce<sup>4+</sup>, has been observed before [16,17] and has also been reported for Pt/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [3]. In view of the higher dispersions, it is thus reasonable that the oxygen storage capacity should also be higher in the Pt/CeO<sub>2</sub>/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst, as observed. From the standpoint of activity, the addition of La<sup>3+</sup> to the Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst affects primarily rich-side HC conversion. A reduction in possible steam reforming activity due to higher Pt dispersion in the catalyst containing La<sup>3+</sup> would

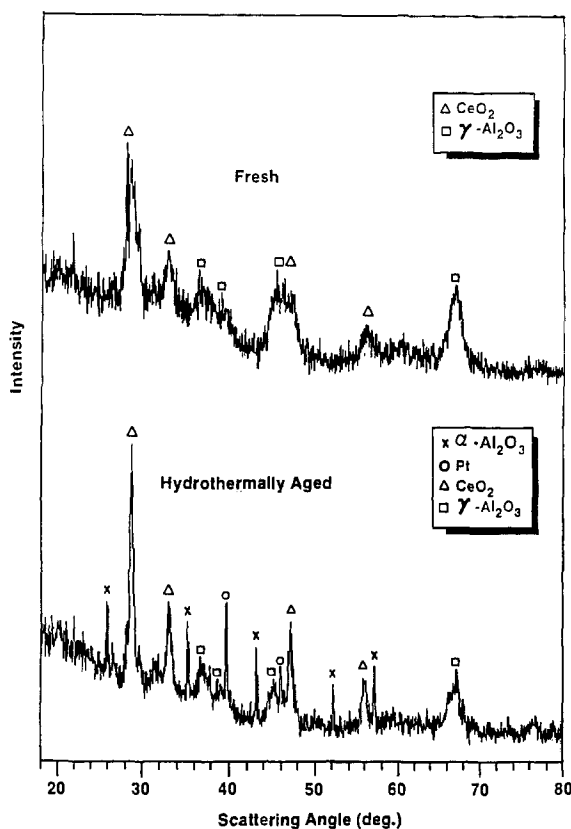


Fig. 5. Diffraction patterns for the fresh (top panel) and hydrothermally aged (bottom panel)  $\text{Pt}/\text{CeO}_2/\text{Al}_2\text{O}_3$  catalyst.

be consistent with this observation if specific activity for steam reforming increases with increasing particle size. This behavior has been observed for reaction of *n*-heptane with steam over  $\text{Rh}/\gamma\text{-Al}_2\text{O}_3$  [18].

Similar effects of  $\text{La}^{3+}$  are also seen after the aging treatments. Activity measurements from thermally aged samples showed the same difference in rich-side HC conversion between the two catalysts as seen in the fresh state. The promotional effect of  $\text{La}^{3+}$  on Pt and  $\text{CeO}_2$  dispersions in these catalysts was also maintained, as shown from both the noble-metal surface area measurements following each pretreatment and the XRD measurements following the hydrothermal treatment. Additional effects beyond a simple promotion of Pt and  $\text{CeO}_2$  dispersions are also evident. Although the TPR results indicate that the presence of  $\text{La}^{3+}$  had no effect on the amount of reducible oxides in the fresh state, the retention of a greater amount of reducibles on the surface after thermal aging suggests that  $\text{La}^{3+}$  may have blocked, to some extent, the interaction of  $\text{CeO}_2$  with  $\text{Al}_2\text{O}_3$  which leads to the stabilization of  $\text{Ce}^{3+}$  [19]. This effect disappears after hydrothermal aging, however. Finally, the XRD data of the hydrothermally aged catalysts indicates that

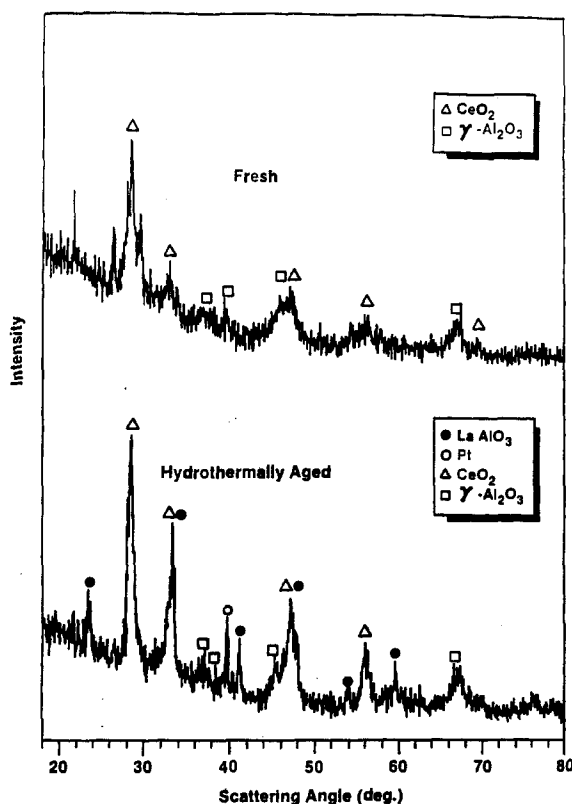


Fig. 6. Diffraction patterns for the fresh (top panel) and hydrothermally aged (bottom panel)  $\text{Pt}/\text{CeO}_2/\text{La}_2\text{O}_3/\text{Al}_2\text{O}_3$  catalyst.

$\text{La}^{3+}$  forms  $\text{LaAlO}_3$  with  $\text{Al}_2\text{O}_3$  and prevents  $\alpha\text{-Al}_2\text{O}_3$  formation while the alpha phase of  $\text{Al}_2\text{O}_3$  is clearly seen in the diffraction pattern from the catalyst without  $\text{La}^{3+}$ .

In summary, this study shows that  $\text{La}^{3+}$  increases the dispersion of  $\text{Pt}$  and  $\text{CeO}_2$  and inhibits to some extent the interaction between  $\text{CeO}_2$  and  $\text{Al}_2\text{O}_3$ . The mechanism by which it inhibits the interaction of  $\text{CeO}_2$  with  $\text{Al}_2\text{O}_3$  appears to involve formation of its own compound with  $\text{Al}_2\text{O}_3$ . Higher dispersions of  $\text{Pt}$  and  $\text{CeO}_2$  and the retention of a greater range of reducible oxides on the surface translate into an improved oxygen storage capacity.

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