# Deactivation of NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts and their improvement for the oxidative coupling of methane

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In the present work, the deactivation of the NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts was studied for the oxidative coupling of methane. Several techniques, such as XPS, XRD, SEM, H<sub>2</sub>-TPR, and flow-reaction, were employed to examine the function of each catalyst component, and its change during the catalytic reaction. NaCl and B<sub>2</sub>O<sub>3</sub> show a synergistic effect on the Fe<sub>2</sub>O<sub>3</sub> surface. B<sub>2</sub>O<sub>3</sub> modifies the oxidative activity of Fe<sub>2</sub>O<sub>3</sub> and makes the first reduction peak of Fe<sub>2</sub>O<sub>3</sub> shift from 490 to 750°C. The NaCl modified B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalyst has high reduction rate, high activity and selectivity at about 750°C. It is demonstrated that the deactivation of the NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts is a complicated process, consisting of chloride loss, sodium change, B<sub>2</sub>O<sub>3</sub> loss, silica deposition and catalyst sintering. The chloride loss enhances the surface basicity, which causes the silica deposition and sodium change, and aggravates the catalyst sintering. The silica deposition and catalyst sintering cause permanent deactivation. The B<sub>2</sub>O<sub>3</sub> loss is not a direct reason for catalyst deactivation. NaCl crystal diluted NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts have a better stability. The deactivated catalyst has a more stable structure. When it is regenerated by impregnating with NaCl again, a more stable catalyst can be obtained.

Keywords: alkali chloride doped ferrous oxides; characterization; deactivation; oxidative activity; oxidative coupling of methane

## 1. Introduction

The large amounts of natural gas (mainly methane) found worldwide have led to extensive recent research programs in the area of direct methane conversion. Although many routes are conceptually possible, the oxidative coupling of methane (OCM) can directly convert methane to useful products without extensive energy consumption [1]. A wide range of materials, such as, alkaline-earth oxides, rare-earth oxides, transition metal oxides, and these doped with alkali metal compounds, were proved to be active catalysts for the oxidative coupling of methane [2,3].

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Having done a lot of work on OCM over alkali, alkaline-earth and rare-earth oxides [4-6], we faced a common problem how to increase catalyst activity and decrease reaction temperature. The oxidation of methane over transition metal oxides is always highly active, but its products are CO and CO<sub>2</sub>, namely the products of deep oxidation. This is because transition metal oxides, especially Fe<sub>2</sub>O<sub>3</sub>, have high oxidative activity to alkanes [7–9]. The strong oxidative reactivity of CH<sub>4</sub> over transition metal oxides such as Fe<sub>2</sub>O<sub>3</sub> indicated that the activation of the C-H  $\sigma$ bond over transition metal oxides is much easier than that over alkaline-earth and rare-earth oxides. Furthermore, the activation of the C-H σ bond is the key step of the OCM reaction. It is the reason that we use Fe<sub>2</sub>O<sub>3</sub> as the main component of the OCM catalysts. However, we have to realize that the C<sub>2</sub> selectivity of Fe<sub>2</sub>O<sub>3</sub> is poor. We expected to improve the C<sub>2</sub> selectivity of Fe<sub>2</sub>O<sub>3</sub> by surface modification, namely making use of the interaction between Fe<sub>2</sub>O<sub>3</sub> and other components to beget a synergistic effect, in order to get better C<sub>2</sub> yield. Professor Amenomiya also pointed out that there was considerable untapped potential in the use of transition metal oxides or composite oxides systems for the OCM [2]. Our results on the OCM over NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> proved that idea and a synergistic effect of NaCl and B2O3 on Fe2O3 was observed.

In our previous paper [10], we have given a more detailed discussion of the synergistic effect of NaCl and  $B_2O_3$  on  $Fe_2O_3$ , the reaction mechanism and the active sites on the catalyst surface. In this paper, the deactivation of the NaCl/ $B_2O_3$ /  $Fe_2O_3$  catalysts will be discussed.

The catalyst stability is an important criterion for practical purpose because the oxidative coupling of methane is a typical high temperature reaction at about 600–800°C. Several simple catalysts can undergo the 500 h life-test [11], but their selectivity and yield are lower than the commercial need. The addition of alkali compounds, especially, alkali metal chlorides, can enhance the activity and the ethylene selectivity. The shortage of the alkali metal compound doped catalysts is their deactivation [12–14].

In this paper, the deactivation of the  $NaCl/B_2O_3/Fe_2O_3$  catalysts was studied. Several techniques, such as flow-reaction, XPS, XRD, SEM, and  $H_2$ -TPR, were employed to examine the function of each catalyst component, and its change during the catalytic reaction. It was found that the catalyst deactivation is a complicated process, comprised of chloride loss, sodium changing,  $B_2O_3$  loss, silica deposition and catalyst sintering. These processes are closely related to each other. Methods to decrease the catalyst deactivation were suggested.

# 2. Experimental

#### 2.1. CATALYST PREPARATION

The catalysts were prepared by two-step impregnation: (a) Known quantities of  $Fe_2O_3$  were impregnated with  $H_3BO_3$  solutions to obtain the  $B_2O_3/Fe_2O_3$  sam-

ples with the B/Fe atomic ratio from 0, 0.01 to 0.3 (labeled as F100, FB01–FB30). (b) Then the  $B_2O_3/Fe_2O_3$  samples were impregnated with NaCl solutions to obtain the NaCl/ $B_2O_3/Fe_2O_3$  catalysts with Na/Fe atomic ratio of 0.25 (labeled as FN25, FBN0125–FBN3025). Samples at different stages of preparation, different periods of reaction and different ways of treatment were collected in order to examine the function of each catalyst component and its change during the catalytic reaction.

## 2.2. FLOW-REACTION

The catalytic reaction was performed in a conventional fixed-bed reactor operated in flow mode at atmospheric pressure. The general reaction conditions were:  $T = 750^{\circ}\text{C}$ ,  $\tau = 0.24$  g s cm<sup>-3</sup>,  $P_{\text{CH}_4}/P_{\text{O}_2} = 4$ ,  $P_{\text{CH}_4} = 32$  kPa, and balanced to atmospheric pressure by helium. The reactant and product analyses were performed by on-line gas chromatography (GC) with a thermal conductivity detector and carbon zeolite columns.

# 2.3. XPS, XRD, SEM AND H2-TPR CHARACTERIZATIONS

XPS data were obtained on a VG ESCALAB MKII photoelectron spectrometer using Al  $K_{\alpha}$  X-ray excitation ( $h\nu=1486.6$  eV). The experimental resolution was better than 0.1 eV. The charge effect was corrected by referring to the 1s level of the background carbon at a binding energy of 284.6 eV.

XRD data were obtained on a Rigaku D/Max-rB X-ray diffractometer using a copper target at  $40 \text{ kV} \times 100 \text{ mA}$  and scanning speed of  $8^{\circ}$ /min.

SEM pictures were obtained on a KyKy-1000B scanning electron photomicrograph after the samples were plated by gold.

H<sub>2</sub>-TPR profiles were recorded at a programmed temperature velocity of 16°C/min after the samples were treated in Ar flow at 700°C for 30 min.

#### 3. Results and discussion

# 3.1. FUNCTIONS OF THE CATALYST COMPONENTS

In the flow-reaction, pure  $Fe_2O_3$  (F100) as a catalyst has high activity but produces only  $CO_2$ ,  $B_2O_3/Fe_2O_3$  (FB20) has poor activity and selectivity. NaCl/ $Fe_2O_3$  (FN25) has high activity but poor selectivity. When 8 wt%  $B_2O_3$  was ground with NaCl as catalyst (BN\*), the  $C_2$  hydrocarbon selectivity is high, but its activity is quite low. Only NaCl and  $B_2O_3$  co-modified  $Fe_2O_3$  catalyst (FBN1525) has high activity and selectivity (table 1). The catalyst performance becomes better as the  $B_2O_3$  content increases. When the additive approaches 15 at%  $B_2O_3$ , the  $C_2$ 

| Catalyst | Conversion (%)  |                | Selectivi | Yield (%)       |                               |       |       |
|----------|-----------------|----------------|-----------|-----------------|-------------------------------|-------|-------|
|          | CH <sub>4</sub> | O <sub>2</sub> | СО        | CO <sub>2</sub> | C <sub>2</sub> H <sub>4</sub> | $C_2$ | $C_2$ |
| F100     | 13.5            | 100            | 0         | 100             | 0                             | 0     | 0     |
| BN*      | 1.2             | 2              | 0         | 2.1             | 23                            | 98    | 1.2   |
| FB20     | 5.9             | 24             | 49.8      | 10.0            | 4.8                           | 40.2  | 2.4   |
| FN25     | 18.2            | 100            | 0.5       | 70              | 15.7                          | 29.1  | 5.4   |
| FBN0125  | 27.7            |                | 0.2       | 50.7            | 37.0                          | 49.1  | 13.6  |
| FBN0525  | 24.2            |                | 12.5      | 21              | 49                            | 66.5  | 16.1  |
| FBN1025  | 22.1            | _              | 18.7      | 5.5             | 54.6                          | 75.8  | 16.8  |
| FBN1525  | 22.7            |                | 18.2      | 5.5             | 58.1                          | 76.3  | 17.4  |
| FBN2025  | 21.4            | 61             | 18.8      | 5.8             | 56.9                          | 75.5  | 16.1  |
| FBN3025  | 19.9            |                | 21.5      | 6.0             | 56.0                          | 65.2  | 13.0  |

Table 1 Performances of the modified Fe<sub>2</sub>O<sub>3</sub> catalysts <sup>a</sup>

hydrocarbon yield and selectivity reach their maxima, 17 and 76%, respectively (fig. 1).

In the H<sub>2</sub>-TPR profiles of the modified Fe<sub>2</sub>O<sub>3</sub> catalysts (fig. 2), pure Fe<sub>2</sub>O<sub>3</sub> (F100) has two reduction peaks at about 490 and 780°C, respectively. The addition of B<sub>2</sub>O<sub>3</sub> adjusts the oxidative activity of Fe<sub>2</sub>O<sub>3</sub>. When the additive is 15 at% B<sub>2</sub>O<sub>3</sub>

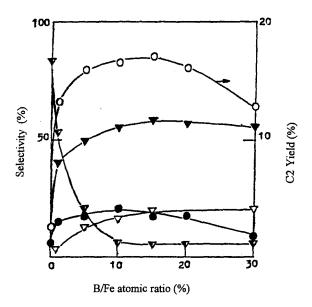


Fig. 1. Optimum amount of  $B_2O_3$  in modified  $Fe_2O_3$  catalysts. ( $\bigcirc$ )  $C_2$  yield, ( $\blacktriangledown$ )  $C_2H_4$  selectivity, ( $\multimap$ )  $C_2H_6$  selectivity, ( $\triangledown$ ) CO selectivity, ( $\blacktriangledown$ ) CO<sub>2</sub> selectivity. NaCl/ $B_2O_3/Fe_2O_3$  catalysts with 25 at% Na/Fe,  $T=750^{\circ}C$ ,  $\tau=0.24$  g s cm<sup>-3</sup>,  $P_{CH_4}/P_{O_2}=4$ ,  $P_{CH_4}=32$  kPa.

<sup>&</sup>lt;sup>a</sup> T = 750°C,  $\tau = 0.21$  g s cm<sup>-3</sup>,  $P_{\text{CH}_4}/P_{\text{O}_2} = 4$ ,  $P_{\text{CH}_4} = 32$  kPa, except for BN\*. BN\* denotes 8 wt% B<sub>2</sub>O<sub>3</sub>/NaCl under reaction conditions of T = 750°C,  $\tau = 1.20$  g s cm<sup>-3</sup>,  $P_{\text{CH}_4}/P_{\text{O}_2} = 4$ , and  $P_{\text{CH}_4} = 32$  kPa.

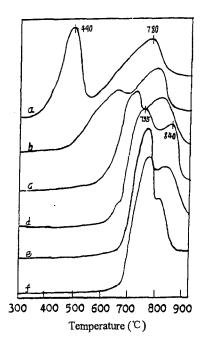


Fig. 2.  $H_2$ -TPR profiles of the modified  $Fe_2O_3$  catalysts. (a) F100, (b) FN25, (c) FBN0525, (d) FB15, (e) FBN1525, (f) FBN3025.

(FB15), the two reduction peaks shift to higher temperatures, at about 755 and 860°C, respectively. NaCl also has some effect on the oxidative activity of Fe<sub>3</sub>O<sub>3</sub> (FN25), but its oxidative activity is still high. The modification of  $B_2O_3/Fe_2O_3$  by NaCl (FBN1525) makes the first reduction peak become more narrow and higher comparing with FB15. The narrow peak width indicates that the NaCl/  $B_2O_3/Fe_2O_3$  catalyst has high reduction velocity at about 750°C. The width of the first peak becomes more narrow as the  $B_2O_3$  content increases. When 15 wt%  $B_2O_3$  is added the width and height of the first peak reach their maxima.

The reduction properties of the modified  $Fe_2O_3$  catalysts well explain the catalytic performance. Pure  $Fe_2O_3$  has high oxidative activity. The addition of  $B_2O_3$  suppresses the oxidative activity of  $Fe_2O_3$ , but no new active species are formed, thus its activity and selectivity are both poor. NaCl cannot inhibit the deep oxidation capability of  $Fe_2O_3$ . When NaCl and  $B_2O_3$  co-modify  $Fe_2O_3$ , the catalyst has high activity and selectivity, and this catalyst has high reduction velocity. The synergic effect of NaCl and  $B_2O_3$  on  $Fe_2O_3$  was described elsewhere [10].

## 3.2. EFFECT OF CHLORIDE AND ITS LOSS

Chloride containing catalysts have high ethylene selectivity. Several papers [15–31] described the significance of chloride and believed that chloride participates in the methane activation and coupling processes. In this paper, it is shown

that the cation, especially the matching of the cation and anion in the salt doped oxide catalysts, is critical to the catalytic performance. The performances of the sodium containing salts and the chloride containing salts modified  $B_2O_3/Fe_2O_3$  catalysts are given in table 2.  $Na_2B_2O_7$  doped catalyst has very low activity. The activities and selectivities of the  $Na_2CO_3$  and  $Na_2P_2O_7$  doped catalysts, or the  $CaCl_2$  and  $LaCl_3$  doped catalysts, are relatively low. Only NaCl doped  $B_2O_3/Fe_2O_3$  catalyst has high activity and selectivity.

In the flow-reaction, pulsing CH<sub>2</sub>Cl<sub>2</sub> into the feed gas, pure Fe<sub>2</sub>O<sub>3</sub> having high activity, produces also mainly CO<sub>2</sub> and some CO. The activity of B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> becomes a little better after the CH<sub>2</sub>Cl<sub>2</sub> injection, but the product is mainly CO. The activity and selectivity of the Na<sub>2</sub>O/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalyst increase significantly after the CH<sub>2</sub>Cl<sub>2</sub> injection, and maintain for more than 30 min, but return to the original levels 1 h later. The same changes were observed when the CH<sub>2</sub>Cl<sub>2</sub> injections were repeated. This shows that (a) chloride is chemisorbed on the catalyst surface, (b) the chemisorbed chloride improves the catalyst performance, and (c) the chemisorbed chloride is lost during the reaction. Those results agree with earlier work [32–34]. From the different effects of CH<sub>2</sub>Cl<sub>2</sub> on the modified Fe<sub>2</sub>O<sub>3</sub>, it is noted that the existence of sodium is significant. The chemisorption of chloride on the catalyst surface was also proved by XPS examination of the samples after CH<sub>2</sub>Cl<sub>2</sub> injection (fig. 3). Sugiyama and co-workers also prove that by using XPS [25,32,33].

The most serious problem of the chloride containing catalysts is their deactivation. In the published papers [15–31], this is attributed to the loss of chloride during reaction. Using XPS to follow the deactivation processes it is noted that the surface concentration of chloride decreases initially by 12.5% but the CH<sub>4</sub> conversion and C<sub>2</sub> selectivity also decrease by 7.2 and 5.4% respectively during the first 10 h of reaction. However, after 40 h of reaction, the surface concentration of chloride

| Table 2  |
|--|
| Performances of different salts modified catalysts |

| Salt  | Conversion<br>of CH <sub>4</sub><br>(%) | Selectiv | Yield (%)<br>C <sub>2</sub> |          |          |                             |
|---|---|----------|-----------------------------|----------|----------|-----------------------------|
|   |   | СО       | $CO_2$                      | $C_2H_4$ | $C_2H_6$ | $\mathcal{O}_{\mathcal{I}}$ |
| NaCl  | 27.9                                    | 22.0     | 7.3                         | 60.3     | 10.5     | 19.7                        |
| LiCl  | 24.1                                    | 26.3     | 17.6                        | 53.0     | 3.0      | 13.5                        |
| CaCl <sub>2</sub>                               | 16.8                                    | 44.0     | 26.3                        | 19.0     | 10.7     | 5.0                         |
| LaCl <sub>3</sub>                               | 4.3                                     | -        | 51.3                        | 15.5     | 33.2     | 2.1                         |
| Na <sub>2</sub> O                               | 15.2                                    | 30.1     | 21.4                        | 12.1     | 36.4     | 7.4                         |
| Na <sub>2</sub> CO <sub>3</sub>                 | 11.5                                    | 22.1     | 40.2                        | 9.5      | 28.2     | 4.3                         |
| Na <sub>4</sub> P <sub>2</sub> O <sub>7</sub> a | 12.7                                    | 21.6     | 63.8                        | 3.9      | 10.7     | 1.9                         |
| Na <sub>2</sub> B <sub>2</sub> O <sub>7</sub> a | 2.1                                     | 54.2     | 27.5                        | 5.2      | 13.1     | 0.4                         |

<sup>&</sup>lt;sup>a</sup> Salts were added to Fe<sub>2</sub>O<sub>3</sub> directly. Other salts were added to B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub>.  $T = 750^{\circ}$ C,  $\tau = 0.24$  g s cm<sup>-3</sup>,  $P_{\text{CH}_4}/P_{\text{O}_2} = 4$ ,  $P_{\text{CH}_4} = 32$  kPa.

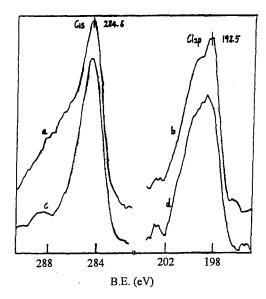


Fig. 3. XPS spectra of FB15 after  $CH_2Cl_2$  treatment. (a) C 1s, (b) Cl 2p, treated at 25°C and  $10^{-6}$  Torr. (c) C 1s, (d) Cl 2p, treated at 600°C and  $10^{-6}$  Torr.

decreases by 62.9%, and CH<sub>4</sub> conversion and C<sub>2</sub> selectivity decrease by 57.4 and 17.6% respectively (table 3). In order to compensate for the chloride loss, CH<sub>2</sub>Cl<sub>2</sub> was added to the feed gas, but no evident effect was observed on the catalyst deactivation. These imply that the catalyst deactivation is not simply due to the chloride loss. The chloride loss is, nevertheless, one of the important deactivation factors; e.g., about 20% of chloride on FBN1025 catalyst was lost as HCl after 40 h of reaction.

#### 3.3. EFFECT OF SODIUM AND ITS CHANGES

The significant effect of sodium on the catalyst performance is evident. XPS data show that the surface sodium concentration remains constant during the first 10 h of reaction. However, it decreases by 55.0% after 40 h of reaction (table 3). It is therefore suggested that sodium change is another factor causing the catalyst

Table 3
Changes of surface composition and catalytic performance <sup>a</sup>

| Reaction<br>time<br>(h) | Conv.<br>of CH <sub>4</sub><br>(%) | Sel.<br>to C <sub>2</sub><br>(%) | Yield<br>of C <sub>2</sub><br>(%) | Surface composition (%) |     |     |    |     |    |  |
|-------------------------|------------------------------------|----------------------------------|-----------------------------------|-------------------------|-----|-----|----|-----|----|--|
|                         |                                    |                                  |                                   | 0                       | Fe  | Cl  | В  | Na  | Si |  |
| 0.5                     | 29.1                               | 65.3                             | 19.0                              | 34                      | 8.1 | 24  | 35 | 4.0 |    |  |
| 10                      | 27.0                               | 61.8                             | 16.7                              | 28                      | 8.2 | 21  | 23 | 4.0 | 15 |  |
| 40                      | 12.4                               | 53.8                             | 6.7                               | 35                      | 4.4 | 8.9 | 10 | 1.8 | 40 |  |

<sup>&</sup>lt;sup>a</sup> FBN1025 catalyst, T = 750°C,  $\tau = 1.2 \text{ g s cm}^{-3}$ ,  $P_{\text{CH}_4}/P_{\text{O}_2} = 4$ ,  $P_{\text{CH}_4} = 32 \text{ kPa}$ .

deactivation [13,35–37]. In a study of the deactivation of Li/MgO catalyst, Kaminsky [12] discovered that it is due to the lithium loss through the evaporation of LiOH, and the formation of Li<sub>2</sub>SiO<sub>3</sub> or LiAlO<sub>2</sub>.

On the NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts, the surface sodium loss occurs also through two ways, i.e., the evaporation of NaCl or NaOH, which can be detected in the reactor downstream the catalyst bed, and the formation of Na<sub>2</sub>FeSi<sub>2</sub>O<sub>6</sub>, which can be detected by XRD in the FBN1025 catalyst after 40 h reaction (fig. 4). The silica is deposited from the corrosion of the quartz reactor wall. NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts do not directly react with quartz at the reaction temperature. As the chloride is lost, the surface basicity increases, which then causes the corrosion of the quartz reactor wall. This chain process would be general in the deactivation of alkali metal chloride containing catalysts.

# 3.4. EFFECT OF B<sub>2</sub>O<sub>3</sub> AND ITS LOSS

The effect of B<sub>2</sub>O<sub>3</sub> is to inhibit the oxidative activity of Fe<sub>2</sub>O<sub>3</sub>. The addition of B<sub>2</sub>O<sub>3</sub> does not create new active sites. Thus the activity of B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> (FB15) is low. NaCl/Fe<sub>2</sub>O<sub>3</sub> (FN25) without modification by B<sub>2</sub>O<sub>3</sub> has a high deep oxidation activity. Only NaCl doped B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalyst (FBN1525) has high activity and selectivity (table 1). It is demonstrated elsewhere [38] that B<sub>2</sub>O<sub>3</sub> and NaCl have a synergistic effect on the Fe<sub>2</sub>O<sub>3</sub> surface, which results in the high activity and selectivity.

From fig. 1 it is seen that the optimum content of  $B_2O_3$  is 15 at%. The catalyst with this  $B_2O_3$  content has a high reduction rate and good catalytic performance. This effect can be understood from the XPS data (fig. 5). After 200 min reaction,

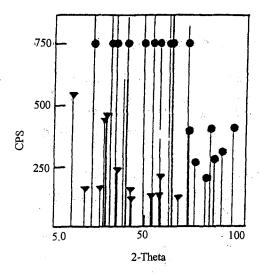


Fig. 4. A new formed compound detected by XRD. (▼) NaFeSi<sub>2</sub>O<sub>6</sub>, (●) Fe<sub>2</sub>O<sub>3</sub>, FBN1025 catalyst after 40 h of reaction.

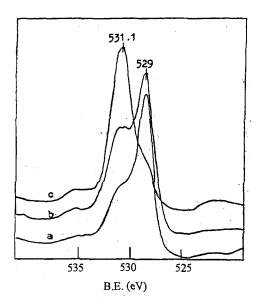


Fig. 5. O 1s XPS spectra of FBN catalysts. (a) FBN0125, (b) FBN1025, (c) FBN3025, after 200 min of reaction.

the lattice oxygen (BE 529 eV) is the major oxygen species on the surface of the FBN0125 catalyst, which has high activity but low  $C_2$  selectivity. On the surface of FBN1025, another surface oxygen species (BE 531.1 eV) modifies the property of the lattice oxygen. This results in better catalytic performance. When the additive oxygen becomes dominant, e.g. on the FBN3025 catalyst, the total activity is quite low (table 1, fig. 5). The C 1s XPS data indicated that there were no carbonates existing over reacted FBN catalysts. So, the O 1s XPS peak at BE 531.1 eV is not due to the existence of carbonates but attributable to a mixture of different species including OH<sup>-</sup>, O<sup>-</sup>, O<sup>2</sup><sub>2</sub> [39].

 $B_2O_3$  is a low melting-point oxide (m.p. 450°C). Its evaporation at the reaction temperature is unavoidable. XPS data show that the  $B_2O_3$  loss during the reaction is serious (table 3). The deposition of silica also causes the  $B_2O_3$  loss. Using XPS to observe the deactivation processes it is noted that the surface concentration of B decreases from 35 to 23%, while that of Si increases from 0 to 15% during the first 10 h reaction. Furthermore, the surface concentration of B decreases to 10% while that of Si increases to 40% (table 3).

#### 3.5. CATALYST SINTERING

The oxidative coupling of methane is a typical high temperature reaction at about  $600-800^{\circ}$ C. The catalyst sintering is expected, especially for the alkali metal compounds doped catalysts. SEM shows that the sintering of the NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts is serious, i.e., the catalyst crystals grew larger during the reaction.

The silica deposition would aggravate the catalyst sintering, which causes the permanent catalyst deactivation.

# 3.6. IMPROVEMENT OF THE CATALYST ACTIVITY

The deactivation of  $NaCl/B_2O_3/Fe_2O_3$  catalysts is a complicated process, comprised of chloride loss, sodium changing,  $B_2O_3$  loss, silica deposition and catalyst sintering. These processes are closely related to each other, e.g., the chloride loss increases the surface basicity, which causes the silica deposition and the sodium change, then aggravates the catalyst sintering. The silica deposition and catalyst sintering cause permanent deactivation. The component loss can be recovered by adding them again. The  $B_2O_3$  loss is special to the deactivation. The effect of  $B_2O_3$  is to inhibit the oxidative activity of  $Fe_2O_3$ . The  $B_2O_3$  loss itself should enhance the catalyst activity with the sacrifice of selectivity. Thus the  $B_2O_3$  loss is not a direct reason for the catalyst deactivation. But the  $B_2O_3$  loss and the silica deposition would change the active sites formed by the synergistic effect between NaCl and  $B_2O_3$ , and then lead to catalyst deactivation.

It would be difficult to avoid the deactivation of the alkali metal chloride doped catalysts. In published papers [13,14,16,17,19–31], chloride containing organic compounds, e.g. bichloromethane, were added to the feed gas. This can compensate the chloride loss on some catalysts. Because the organic compounds decompose to CO, its concentration should be limited. On the NaCl/B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalysts the addition of CH<sub>2</sub>Cl<sub>2</sub> to the feed gas does not show evident effect on the original rapid catalyst deactivation.

To inhibit the catalyst sintering and chloride loss, the FBN1025 catalyst was ground with NaCl to prepare a NaCl diluted catalyst. Its activity and stability are significantly improved (fig. 6). The activity reaches a stable level after 1 h which was maintained for more than 10 h with a high ethylene selectivity.

The deactivated FBN1025 catalyst was regenerated by impregnating with NaCl again. It is shown that the regenerated catalyst has high stability and selectivity (fig. 7). The methane conversion and  $C_2$  hydrocarbon selectivity maintain at 15 and 82%, respectively, at the reaction conditions:  $T=750^{\circ}\mathrm{C}$ ,  $\tau=0.24~\mathrm{g~s~cm^{-3}}$ ,  $P_{\mathrm{CH_4}}/P_{\mathrm{O_2}}=4$  and  $P_{\mathrm{CH_4}}=32~\mathrm{kPa}$ . The high stability of the regenerated catalyst would be due to the slow catalyst re-sintering and the slow silica re-deposition. After the first run, the deactivated catalyst has a more stable structure, from which a more stable catalyst can be obtained.

# 4. Conclusion

Pure Fe<sub>2</sub>O<sub>3</sub> has a high oxidation activity. NaCl and B<sub>2</sub>O<sub>3</sub> have a synergistic effect on the Fe<sub>2</sub>O<sub>3</sub> surface. B<sub>2</sub>O<sub>3</sub> inhibits the oxidative activity of Fe<sub>2</sub>O<sub>3</sub>, and makes the first reduction peak of Fe<sub>2</sub>O<sub>3</sub> shift from 490 to 750°C. The NaCl modi-

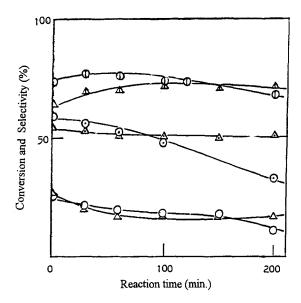


Fig. 6. Effect of NaCl dilution on the performance. ( $\bigcirc$ ) CH<sub>4</sub> conversion, ( $\bigcirc$ ) C<sub>2</sub>H<sub>4</sub> selectivity, ( $\bigcirc$ ) C<sub>2</sub> selectivity, FBN1025 catalyst. ( $\triangle$ ) CH<sub>4</sub> conversion, ( $\triangle$ ) C<sub>2</sub>H<sub>4</sub> selectivity, ( $\triangle$ ) C<sub>2</sub> selectivity, NaCl diluted FBN1025 catalyst,  $T=750^{\circ}\text{C}$ ,  $\tau=1.2$  g s cm<sup>-3</sup>,  $P_{\text{CH}_4}/P_{\text{O}_2}=4$ ,  $P_{\text{CH}_4}=32$  kPa.

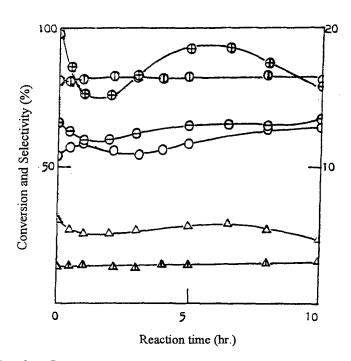


Fig. 7. Stabilities of the FBN1025 and reactivated FBN1025 catalysts. ( $\triangle$ ) CH<sub>4</sub> conversion, ( $\ominus$ ) C<sub>2</sub> selectivity, ( $\ominus$ ) C<sub>2</sub> yield, FBN1025 catalyst. ( $\triangle$ ) CH<sub>4</sub> conversion, ( $\bigcirc$ ) C<sub>2</sub> selectivity, ( $\bigcirc$ ) C<sub>2</sub> yield, reactivated FBN1025 catalyst.

fied B<sub>2</sub>O<sub>3</sub>/Fe<sub>2</sub>O<sub>3</sub> catalyst has a high reduction rate, high activity and selectivity at about 750°C.

The deactivation of the  $NaCl/B_2O_3/Fe_2O_3$  catalysts is a complicated process, consisting of chloride loss, sodium changing,  $B_2O_3$  loss, silica deposition and catalyst sintering. These processes are closely related to each other. The chloride loss enhances the surface basicity, which causes the silica deposition and sodium change, and then aggravates the catalyst sintering. The silica deposition and the catalyst sintering cause permanent deactivation. The  $B_2O_3$  loss is not a direct reason for catalyst deactivation.

NaCl crystal diluted  $NaCl/B_2O_3/Fe_2O_3$  catalysts have better stability. The deactivated catalyst has a more stable structure. When it is regenerated by impregnation with NaCl again, a more stable catalyst can be obtained.

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