# Catalytic performance of indium-supported TiO<sub>2</sub>–ZrO<sub>2</sub> for the selective reduction of nitrogen monoxide in the presence of oxygen

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The catalytic activity of indium-supported  $TiO_2$ – $ZrO_2$  binary metal oxide for the selective reduction of NO with propene in the presence of oxygen was investigated. The supported indium caused a drastic enhancement of NO reduction activity of  $TiO_2$ – $ZrO_2$ . It was suggested that the "dispersed phase" of indium oxide, which is reduced at lower temperature in temperature-programmed reduction (TPR), is responsible for the high activity. Propene served as the most efficient reducing agent, while oxygenated hydrocarbons were not good ones. A reaction mechanism was proposed that  $N_2$  is formed through the reaction of propene and  $NO_2$ , which was formed on the acid sites of  $TiO_2$ – $ZrO_2$ , on the indium sites.

Keywords: nitrogen monoxide, selective reduction, binary oxide, In-supported TiO2-ZrO2, TPR

### 1. Introduction

The selective catalytic reduction of nitrogen oxides (NOx) with hydrocarbons in the presence of excess oxygen is attracting much attention from a viewpoint of practical applications to the deNOx system of diesel and lean-burn gasoline engine exhausts [1]. Many catalysts for this reaction have been reported after Cu ionexchanged ZSM-5 catalyst was discovered by Held et al. [2] and Iwamoto et al. [3], following patent literature [4,5]. Although most of them were related to zeolitebased catalysts such as Ce-[6], Pt-[7], H-ZSM-5[8], Cobeta [9] and so on, our group found that single metal oxides such as Al<sub>2</sub>O<sub>3</sub> [10] and transition metal-supported alumina [11] also catalyze this reaction. Furthermore, we reported that several binary oxides showed higher activity than their corresponding single metal oxides for NO reduction by propane [12].

Hosose et al. [13] reported that the addition of copper to  $SiO_2$ – $Al_2O_3$  binary oxide enhanced the catalytic activity for NO reduction by ethene. There are, however, few reports concerning the effect of metal additives on the activity of binary oxides. Recently, we reported that silver-supported  $TiO_2$ – $ZrO_2$  catalysts showed high activity for NO reduction by propene in the presence of oxygen and confirmed that  $TiO_2$ – $ZrO_2$  binary oxide can be used as a good catalytic support for this reaction [14].

In many cases the transition metals are loaded on metal oxide supports as an active component to improve the NO reduction activity. Miyadera and Yoshida [15] reported, however, that indium, which is not a transition metal, supported on alumina showed a high catalytic activity for NO reduction by propene. Kikuchi and

Yogo [16] also reported that addition of gallium and indium, which are group IIIA metals, to H-ZSM-5 caused an enhancement of the catalytic activity for NO reduction by methane. Hence, some base metals in addition to transition metals also seem to be effective additives toward the title reaction.

In the present work, we investigated the additive effect of indium on the activity of  $\text{TiO}_2\text{-}Z\text{rO}_2$  binary oxide for the selective reduction of NO with propene in the presence of excess oxygen. Here, we selected  $\text{TiO}_2\text{-}Z\text{rO}_2$  as the support because of its high BET surface area, which enables preparation of highly dispersed metal supported catalysts. The presence of solid acid or base property on  $\text{TiO}_2\text{-}Z\text{rO}_2$  and the higher heat resistance compared to  $\text{TiO}_2$  and  $\text{ZrO}_2$  are other reasons for its selection.

In the course of our study, we found that indium enhances the NO reduction activity of TiO<sub>2</sub>–ZrO<sub>2</sub> more than silver reported previously [14]. Accordingly, we report here the detailed experimental results on the role of indium for this reaction and would like to discuss a possible reaction mechanism. The efficiency of various hydrocarbons as a reducing agent was also examined.

### 2. Experimental

# 2.1. Catalyst preparation

TiO<sub>2</sub>–ZrO<sub>2</sub> binary oxide with a molar ratio of unity was prepared according to our previous paper [14]. In brief, the binary oxide was obtained by hydrolyzing a solution containing titanium(IV) tetraisopropoxide and zirconium(IV) tetrapropoxide in 2-propanol, followed by drying at 110°C and calcination at 500°C for 5 h in air

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stream. Indium-supported catalysts were prepared by immersing  $TiO_2$ – $ZrO_2$  powder in an aqueous solution of  $In(NO_3)_3$ - $2H_2O$ , followed by drying and calcination at  $500^{\circ}$ C for 5 h in flowing air. Indium loading was changed from 2 wt% to 15 wt% as In metal.

# 2.2. Catalytic activity measurements

The catalytic activity was measured with a fixed-bed flow reactor by passing a reactant gas containing 900 ppm NO, 10% O<sub>2</sub>, a reducing agent and helium as the balance gas at a rate of  $66 \text{ cm}^3 \text{ min}^{-1}$  over 0.2 g of catalyst. CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>3</sub>H<sub>8</sub>, C<sub>3</sub>H<sub>6</sub>, CH<sub>3</sub>OH, C<sub>2</sub>H<sub>5</sub>OH, 1-C<sub>3</sub>H<sub>7</sub>OH, 2-C<sub>3</sub>H<sub>7</sub>OH and (CH<sub>3</sub>)<sub>2</sub>CO were used as the reducing agent. In order to investigate a reaction pathway, NO<sub>2</sub> (930 ppm) reduction and propene (860 ppm) oxidation by O<sub>2</sub> (10%) were also carried out. The analysis of the effluent gas was made by gas chromatographs equipped with a Molecular Sieve 5A column (for the analysis of N<sub>2</sub>, CO and CH<sub>4</sub>) and a Porapak Q column (for that of CO<sub>2</sub>, N<sub>2</sub>O, C<sub>2</sub>H<sub>4</sub>, C<sub>3</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>). The reaction temperature was changed with a step of  $50^{\circ}$ C from  $500 \text{ to } 200^{\circ}$ C.

### 2.3. Catalyst characterization

BET surface area was measured with a conventional flow apparatus (Shimadzu, Flowsorb II 2300) by nitrogen adsorption at  $-196^{\circ}C$ . The crystal structure was identified by XRD (Shimadzu XD-1) measurements using Cu  $K\alpha$  radiation at 40 kV and 40 mA.

TPR (temperature-programmed reduction) measurements were carried out to estimate the reduction behavior of the indium-supported catalysts. Before the TPR measurement, 0.05 g of the catalyst was placed in a quartz tube reactor and oxidized at 500°C for 1 h in flowing air. 10 vol%  $H_2\text{--Ar}$  gas mixture was used as a reducing gas with a flow rate of 30 ml min $^{-1}$  and the

temperature of the catalyst bed was raised at a heating rate of  $5^{\circ}$ C min<sup>-1</sup>. After the outlet gas from the catalyst bed was passed through a silica gel column to eliminate  $H_2$ O produced by the TPR operation, the difference in the  $H_2$  concentration between at the inlet and at the outlet of the reactor was detected by a thermal conductivity detector.

## 3. Results and discussion

# 3.1. NO reduction activity of indium-supported TiO<sub>2</sub>–ZrO<sub>2</sub>

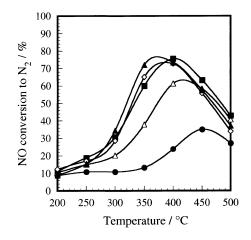
Figure 1 shows the catalytic activity of indium-supported  $TiO_2$ – $ZrO_2$  for NO reduction by propene in the presence of 10% oxygen. It is clear that NO conversion to  $N_2$  on  $TiO_2$ – $ZrO_2$  was enhanced drastically from 25 to 60% at  $400^{\circ}$ C by addition of 2 wt% of indium. Indium loading of more than 5 wt%, however, did not cause a further enhancement of the maximum NO conversion, although the temperature giving the maximum NO conversion shifted to a lower temperature region. The propene oxidation activity increased with indium loading up to 10 wt%, although propene conversion to COx on 15 wt%  $In/TiO_2$ – $ZrO_2$  was almost the same as that on 10 wt%  $In/TiO_2$ – $ZrO_2$ .

The ratio of NO conversion to propene conversion can be regarded as the selectivity of this reaction. We calculated the selectivity for NO reduction, defined as the following equation:

selectivity

 $= \frac{\text{number of NO molecules reduced to N}_2}{\text{number of C}_3\text{H}_6 \text{ molecules oxidized to COx}}$ 

In table 1 are summarized the selectivities on  $In/TiO_2-ZrO_2$  at 350 and 400°C along with the conversions of NO to  $N_2$  and those of propene to COx. The selectivity on



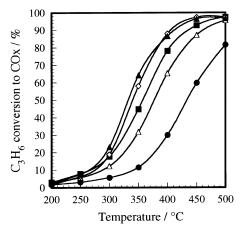


Figure 1. Additive effect of indium in the catalytic activity of  $TiO_2$ – $ZrO_2$  for the selective reduction of NO with propene. Conditions: NO = 900 ppm,  $C_3H_6 = 860$  ppm,  $O_2 = 10\%$ , catalyst weight = 0.2 g, gas flow rate =  $66 \text{ cm}^3 \text{ min}^{-1}$ . ( $\bullet$ )  $TiO_2$ – $ZrO_2$ , ( $\triangle$ ) 2 wt%  $In/TiO_2$ – $ZrO_2$ , ( $\bullet$ ) 5 wt%  $In/TiO_2$ – $ZrO_2$ , ( $\bullet$ ) 10 wt%  $In/TiO_2$ – $ZrO_2$ , ( $\bullet$ ) 15 wt%  $In/TiO_2$ – $ZrO_2$ .

Catalyst	Reaction temperature (°C)	NO conversion to N <sub>2</sub> (%)	$C_3H_6$ conversion to $COx$ (%)	Selectivity
TiO <sub>2</sub> –ZrO <sub>2</sub>	350	13.2	11.5	1.22
	400	23.8	30.0	0.85
$2\% In/TiO_2-ZrO_2$	350	37.9	31.7	1.32
	400	61.3	65.4	1.00
$5\% \operatorname{In/TiO_2-ZrO_2}$	350	60.0	44.8	1.46
	400	75.4	78.1	1.03
$10\%  In/TiO_2 - ZrO_2$	350	65.0	57.9	1.24
	400	72.7	87.9	0.89
$15\% In/TiO_2-ZrO_2$	350	72.1	64.2	1.20
	400	73.4	86.5	0.89

Table 1
Conversions and selectivity over In/TiO<sub>2</sub>–ZrO<sub>2</sub> <sup>a</sup>

In/TiO<sub>2</sub>–ZrO<sub>2</sub> increased gradually with indium loading and reached a maximum at about 5 wt%. This means that indium loaded on TiO<sub>2</sub>–ZrO<sub>2</sub> accelerates the reduction of nitrogen oxides by propene. However, in the region above 10 wt% of indium loading, the selectivity turned to a decrease. This would be ascribed to the promotion of the direct oxidation of propene by oxygen, which decreases the selectivity, by excess amounts of indium.

# 3.2. Morphology of indium species supported on $TiO_2$ – $ZrO_2$

BET surface area of In/TiO<sub>2</sub>–ZrO<sub>2</sub> catalysts was measured together with that of the support. The results are summarized in table 2. The BET surface area of TiO<sub>2</sub>–ZrO<sub>2</sub> was about 280 m<sup>2</sup> g<sup>-1</sup>, but it decreased monotonously with increasing indium loading. This can be attributed to a blockage of the pores of TiO<sub>2</sub>–ZrO<sub>2</sub> by supported indium. In order to examine the crystallite structure of the supported indium, XRD measurements were carried out. As can be seen in figure 2, no diffraction peaks assigned to indium compounds were observed in the XRD patterns of all the In/TiO<sub>2</sub>–ZrO<sub>2</sub> catalysts. Indium seems to be highly dispersed on TiO<sub>2</sub>–ZrO<sub>2</sub> support.

Figure 3 shows the result of TPR measurements carried out to clarify the morphology of indium on TiO<sub>2</sub>-ZrO<sub>2</sub>. Two reduction peaks in the temperature regions between 200 and 300°C and above 500°C were observed in the TPR profiles of indium-supported TiO2-ZrO2 catalysts. These peaks are attributed to the reduction of supported indium oxide, because no outstanding reduction peaks were detected in the TPR profile of TiO<sub>2</sub>-ZrO<sub>2</sub> itself below 500°C. It is considered that indium oxide supported on TiO<sub>2</sub>–ZrO<sub>2</sub> consists of two species: one is a dispersed phase species reducible at low temperature and the other is a bulk phase species reducible at high temperature. On the other hand, pure  $In_2O_3$  as a standard sample did not show clear reduction peaks, but was reduced slowly in the temperature region above 500°C. This is probably because In<sub>2</sub>O<sub>3</sub> is made up of only large particles of the "bulk phase", suggested by its low BET surface area  $(74 \,\mathrm{m}^2 \,\mathrm{g}^{-1})$ .

Apparently, the temperature of both reduction peaks shifted to low temperature region with indium loading up to 10 wt%, and the reduction behavior of In species on 15 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub> was almost the same as that on 10 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>. This fact suggests that the indium dispersion does not change more than 10 wt% indium loading. The relative peak areas of the peak around

Table 2
BET surface areas and relative peak areas of the peak around 250°C in TPR profiles of In/TiO <sub>2</sub> –ZrO <sub>2</sub>

Catalyst	BET surface area (m <sup>2</sup> g <sup>-1</sup> )	TPR p	rofiles	
		temperature of peak below 500°C (°C)	relative area of the peak around $250^{\circ}\mathrm{C}^{\mathrm{b}}$	
TiO <sub>2</sub> –ZrO <sub>2</sub>	284	n.d. a	=	
$2\% \operatorname{In/TiO_2-ZrO_2}$	212	275	100	
$5\% \operatorname{In/TiO_2-ZrO_2}$	206	250	176	
$10\% \operatorname{In/TiO_2-ZrO_2}$	184	230	201	
$15\% \operatorname{In/TiO}_2 - \operatorname{ZrO}_2$	162	230	198	
$In_2O_3$	74	n.d. <sup>a</sup>	_	

<sup>&</sup>lt;sup>a</sup> n.d. means that the peak was not detected in the temperature region below 500°C.

<sup>&</sup>lt;sup>a</sup> Conditions: NO = 900 ppm,  $C_3H_6 = 860$  ppm,  $O_2 = 10\%$ , catalyst weight = 0.2 g, gas flow rate =  $66 \text{ cm}^3 \text{ min}^{-1}$ .

 $<sup>^</sup>b$  Normalized based on the peak area of  $2\%\,In/TiO_2-ZrO_2.$ 

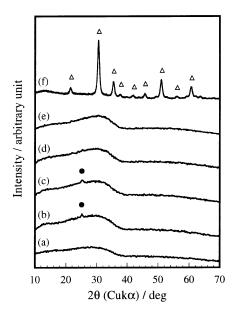


Figure 2. X-ray diffraction patterns of (a)TiO<sub>2</sub>–ZrO<sub>2</sub>, (b) 2 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>, (c) 5 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>, (d) 10 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>, (e) 15 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub> and (f) pure In<sub>2</sub>O<sub>3</sub> as standard. ( $\bullet$ ) TiO<sub>2</sub> (anatase), ( $\triangle$ ) In<sub>2</sub>O<sub>3</sub>.

 $250^{\circ}$ C, normalized based on the peak area of 2 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>, were also summarized in table 2. It is noteworthy that the relative peak area increased gradually up to 10 wt% of In loading. This tendency is consistent with that of NO reduction activity. On the basis of these results, we concluded that the "dispersed phase" of

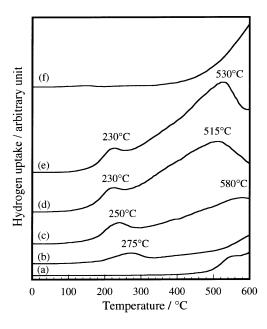


Figure 3. TPR profiles of (a)  $TiO_2$ – $ZrO_2$ , (b) 2 wt%  $In/TiO_2$ – $ZrO_2$ , (c) 5 wt%  $In/TiO_2$ – $ZrO_2$ , (d) 10 wt%  $In/TiO_2$ – $ZrO_2$ , (e) 15 wt%  $In/TiO_2$ – $ZrO_2$  and (f) pure  $In_2O_3$  (standard) after oxidation at 500°C for 1 h. Conditions: catalyst weight = 0.05 g, gas flow rate = 30 cm<sup>3</sup> min<sup>-1</sup>, heating rate = 10°C min<sup>-1</sup>, reducing gas: 10%  $H_2$ –Ar.

indium oxide, which is reduced at low temperature, is the active species for NO reduction and is responsible for the activity enhancement.

## 3.3. Efficiency of the reducing agent

The efficiency of various reducing agents for the selective reduction of NO over 5 wt% In/TiO2-ZrO2 was investigated. The results are summarized in table 3. For hydrocarbons, methane hardly promoted NO reduction. Ethene and propane were not good reducing agents, either. NO reduction proceeded at relatively high temperatures with these three hydrocarbons. Among hydrocarbons tested here, propene served as the most efficient reducing agent. Oxygenated hydrocarbons did not serve as an efficient reducing agent for NO reduction, compared with hydrocarbons. This would be because they are oxidized by oxygen more easily than their corresponding hydrocarbons. The efficiency increased in the sequence of methanol < ethanol < 1propanol = acetone < 2-propanol, although exact comparison of the efficiency is impossible because of the different C/NO ratios.

### 3.4. Reaction mechanism

The reaction pathway of NO reduction by propene over 5 wt% In/TiO2-ZrO2 was investigated by measuring the activity for several unit reactions. The reactivity of NO and NO<sub>2</sub> was compared first. Figure 4 presents the reaction results on In/TiO<sub>2</sub>-ZrO<sub>2</sub> and on TiO<sub>2</sub>-ZrO<sub>2</sub>. The reactivity of NO<sub>2</sub> is slightly higher than that of NO at temperatures below 350°C. These facts suggest the participation of NO<sub>2</sub> as an intermediate in NO reduction. It was reported that one of the roles of supported metals is to promote NO oxidation to NO<sub>2</sub>, as in the case of Co in Co/Al<sub>2</sub>O<sub>3</sub> [17] and Ce in Ce-ZSM-5 [7]. In this work, however, the role of indium on In/TiO<sub>2</sub>-ZrO<sub>2</sub> is not to accelerate NO oxidation, because NO<sub>2</sub> conversion to N2 on TiO2-ZrO2 was lower than NO conversion to  $N_2$  on  $In/TiO_2$ – $ZrO_2$ . This consideration is also supported by the experimental results for NO oxidation to NO<sub>2</sub> carried out on both TiO<sub>2</sub>–ZrO<sub>2</sub> and In/ TiO<sub>2</sub>–ZrO<sub>2</sub>. The conversion of NO to NO<sub>2</sub> at 400°C was about 28% for both catalysts. Clearly, this means that the supported indium does not catalyze NO oxidation to  $NO_2$ .

Since the activation of hydrocarbons by NOx and/or  $O_2$  is considered to be another role of supported indium, we examined next the propene conversion to COx for the reaction system of NO +  $C_3H_6 + O_2$ ,  $C_3H_6 + O_2$  and NO<sub>2</sub> +  $C_3H_6 + O_2$ . The results are shown in figure 5. Apparently, the catalytic activity of In/TiO<sub>2</sub>–ZrO<sub>2</sub> for propene oxidation by  $O_2$  was almost the same as that of TiO<sub>2</sub>–ZrO<sub>2</sub>, suggesting that propene combustion by oxygen occurs predominantly on TiO<sub>2</sub>–ZrO<sub>2</sub> and that indium does not promote this step. However, the catalyt-

Table 3
Efficiency of various reducing agents for the selective reduction of NO over 5 wt% In/TiO <sub>2</sub> -ZrO <sub>2</sub> a

Reductant	N	NO conversion to $N_2$ (%) (HC conversion to COx (%))				
	300°C	350°C	400°C	450°C	500°C	
CH <sub>4</sub>	2.3	2.7	4.0	5.4	6.7	
2790 ppm	(0.9)	(1.2)	(2.0)	(5.8)	(13)	
$\mathrm{C_2H_4}$	8.4	14	22	30	28	
1410 ppm	(3.1)	(5.9)	(12)	(24)	(46)	
$C_3H_6$	31	60	75	63	43	
860 ppm	(18)	(45)	(78)	(93)	(97)	
$C_3H_8$	2.1	6.3	14	25	25	
890 ppm	(0.6)	(3.2)	(10)	(27)	(50)	
CH₃OH	2.3	2.2	2.3	2.2	2.4	
510 ppm	(98)	(100)	(100)	(99)	(98)	
$C_2H_5OH$	15	22	21	11	8.4	
450 ppm	(55)	(79)	(93)	(94)	(98)	
1-C <sub>3</sub> H <sub>7</sub> OH	19	28	29	17	3.6	
550 ppm	(49)	(78)	(98)	(99)	(99)	
2-C <sub>3</sub> H <sub>7</sub> OH	16	32	41	33	19	
550 ppm	(26)	(65)	(91)	(99)	(100)	
(CH <sub>3</sub> ) <sub>2</sub> CO	18	28	32	19	9.2	
680 ppm	(51)	(81)	(99)	(100)	(100)	

<sup>&</sup>lt;sup>a</sup> Conditions: NO = 900 ppm,  $O_2 = 10\%$ , catalyst weight = 0.2 g; gas flow rate = 66 cm<sup>3</sup> min<sup>-1</sup>.

ic activity of  $TiO_2$ – $ZrO_2$  for propene oxidation was depressed considerably by the presence of NO or  $NO_2$ . On the other hand, the propene conversion to COx on  $In/TiO_2$ – $ZrO_2$  is almost the same for all the reaction systems. These results agree with the selectivity increase for NO reduction to  $N_2$  by addition of indium, as described above. On the basis of these results, it is considered that

propene is activated by the reaction with NOx (NO or NO<sub>2</sub>) mainly on indium.

It is well known that TiO<sub>2</sub>–ZrO<sub>2</sub> exhibits high surface acidity by a charge imbalance based on the generation of Ti–O–Zr bonding [18]. Hence, it is considered that acid sites of TiO<sub>2</sub>–ZrO<sub>2</sub> play an important role for this reaction. There are some reports that the role of acid sites is

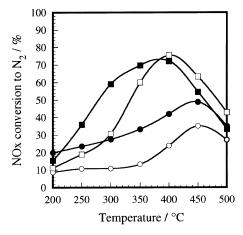


Figure 4. Comparison of reactivity between NO  $(\bigcirc, \square)$  and NO<sub>2</sub>  $(\bullet, \blacksquare)$  for the selective reduction over TiO<sub>2</sub>–ZrO<sub>2</sub>  $(\bigcirc, \bullet)$  and 5 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub>  $(\square, \blacksquare)$ . Conditions: NO = 900 ppm or NO<sub>2</sub> = 930 ppm, C<sub>3</sub>H<sub>6</sub> = 860 ppm, O<sub>2</sub> = 10%, catalyst weight = 0.2 g, gas flow rate = 66 cm<sup>3</sup> min<sup>-1</sup>.

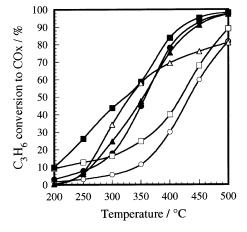


Figure 5. Comparison of the propene conversion to COx for the reaction system of NO + C<sub>3</sub>H<sub>6</sub> + O<sub>2</sub> ( $\bigcirc$ ,  $\bullet$ ), C<sub>3</sub>H<sub>6</sub> + O<sub>2</sub> ( $\triangle$ ,  $\blacktriangle$ ) and NO<sub>2</sub> + C<sub>3</sub>H<sub>6</sub> + O<sub>2</sub> ( $\square$ ,  $\blacksquare$ ) over TiO<sub>2</sub>–ZrO<sub>2</sub> ( $\bigcirc$ ,  $\triangle$ ,  $\square$ ) and 5 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub> ( $\bullet$ ,  $\blacktriangle$ ,  $\blacksquare$ ). The reaction conditions are the same as for figure 4.

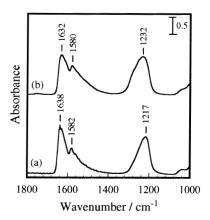


Figure 6. FT-IR spectra of adsorbed species formed on (a) TiO<sub>2</sub>–ZrO<sub>2</sub> and (b) 5 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub> after exposure to a mixture of NO (5 Torr) + O<sub>2</sub> (30 Torr) at room temperature for 30 min, and then evacuation at room temperature for 30 min.

to promote NO oxidation step. For instance, Kikuchi and Yogo reported that acid sites of Ga-ZSM-5, In-ZSM-5 and H-ZSM-5 are responsible for NO oxidation activity, although the detailed mechanism is not clear [16]. In the present study, it is presumed that the acid (or acid-base pair) sites of TiO2-ZrO2 catalyze NO oxidation and NO<sub>2</sub> formed thus participates directly in the overall NO reduction. In order to examine surface adsorbed species formed on TiO2-ZrO2 and In/TiO2- $ZrO_2$  after exposure to  $NO + O_2$ , we carried out in situ IR measurements. FT-IR spectra were recorded in the same manner described elsewhere [19]. A reaction gas composed of NO (5 Torr) and O<sub>2</sub> (30 Torr) was used. As given in figure 6, similar FT-IR spectra were obtained on both TiO<sub>2</sub>–ZrO<sub>2</sub> and In/TiO<sub>2</sub>–ZrO<sub>2</sub>. All the IR peaks observed here were assigned to NO<sub>3</sub> species [20]. Since the peak position and the relative peak intensity are almost the same on both catalysts,  $NO_2$ -like ( $NO_3^-$ ) species seems to be formed mainly on TiO<sub>2</sub>–ZrO<sub>2</sub>.

We also carried out the following experiment concerning the effect of Na additive, which is poisonous material inhibiting the acid sites, to In/TiO<sub>2</sub>–ZrO<sub>2</sub>, in

order to get detailed information on the role of acid sites of TiO<sub>2</sub>–ZrO<sub>2</sub>. Na-modified TiO<sub>2</sub>–ZrO<sub>2</sub>, abbreviated as  $Na/TiO_2-ZrO_2$ , was prepared by immersing  $TiO_2-ZrO_2$ powder in an aqueous solution of Na<sub>2</sub>CO<sub>3</sub>, followed by drying and calcination at 500°C in flowing air. The content of Na was fixed at 1 wt%. Then, In/Na/TiO<sub>2</sub>-ZrO<sub>2</sub> was prepared by the impregnation method described above in the experimental section. The loading of In was fixed at 5 wt%. BET surface area of this catalyst was found to be  $185 \text{ m}^2 \text{ g}^{-1}$ , which is almost the same as that of In/TiO<sub>2</sub>-ZrO<sub>2</sub>. We carried out NO-C<sub>3</sub>H<sub>6</sub>-O<sub>2</sub> and NO<sub>2</sub>-C<sub>3</sub>H<sub>6</sub>-O<sub>2</sub> reactions over In/Na/TiO<sub>2</sub>-ZrO<sub>2</sub>. The reaction results as well as those of In/TiO2-ZrO2 are summarized in table 4. Obviously, the addition of Na into In/TiO<sub>2</sub>-ZrO<sub>2</sub> caused a drastic loss of NO reduction activity of In/TiO<sub>2</sub>–ZrO<sub>2</sub> over the whole temperature range, indicating that Na-additive inhibited important steps in this reaction. We think that Na-additive depressed the de-NOx activity of In/TiO<sub>2</sub>–ZrO<sub>2</sub> by weakening the acidity of TiO<sub>2</sub>–ZrO<sub>2</sub>, because no change in BET surface area of TiO2-ZrO2 was observed before and after the addition of Na. If all of the reaction steps take place on the indium sites, NO2 reduction activity of In/TiO<sub>2</sub>–ZrO<sub>2</sub> and In/Na/TiO<sub>2</sub>–ZrO<sub>2</sub> would be almost the same. However, the former was much higher than the latter. Consequently, we concluded that TiO<sub>2</sub>–ZrO<sub>2</sub> plays an important role to form NO2 and to concentrate NO<sub>2</sub> as NO<sub>3</sub> on its acid site, and that NO<sub>2</sub> formed thus reacts with propene to form N<sub>2</sub> over In sites. The proposed reaction pathway is illustrated in scheme 1.

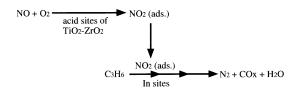
### 4. Conclusions

The catalytic performance of indium-supported TiO<sub>2</sub>–ZrO<sub>2</sub> binary metal oxide for the selective reduction of NO with propene was investigated. The supported indium promoted drastically the activity of TiO<sub>2</sub>–ZrO<sub>2</sub> for the selective reduction of NO. Optimum indium loading was at 5 wt%. It was suggested that a highly dispersed indium oxide phase is responsible for

Table 4
The influence of Na additive on the catalytic activity of 5 wt% In/TiO<sub>2</sub>–ZrO<sub>2</sub> for NO reduction and NO<sub>2</sub> reduction by propene <sup>a</sup>

Catalyst	Reaction	No	NOx conversion to $N_2$ (%) ( $C_3H_6$ conversion to $COx$ (%))				
		300°C	350°C	400°C	450°C	500°C	
5% In/TiO <sub>2</sub> –ZrO <sub>2</sub>	$NO + C_3H_6 + O_2$	31	60	75	63	43	
		(18)	(45)	(78)	(93)	(97)	
	$NO_2 + C_3H_6 + O_2$	59	70	72	54	33	
		(44)	(59)	(84)	(95)	(98)	
5% In/1% Na/TiO <sub>2</sub> –ZrO <sub>2</sub>	$NO + C_3H_6 + O_2$	16	27	38	40	34	
		(6.4)	(18)	(38)	(60)	(79)	
	$NO_2 + C_3H_6 + O_2$	18	39	45	49	47	
		(10)	(25)	(45)	(62)	(80)	

<sup>&</sup>lt;sup>a</sup> Conditions: NO = 900 ppm or NO<sub>2</sub> = 930 ppm,  $C_3H_6 = 860$  ppm,  $O_2 = 10\%$ , catalyst weight = 0.2 g; gas flow rate = 66 cm<sup>3</sup> min<sup>-1</sup>.



Scheme 1. Proposed reaction pathway of the selective reduction of NO with propene over In/TiO<sub>2</sub>–ZrO<sub>2</sub>.

the activity enhancement. Although methane, ethane, propane and alcohols were not good reductants, propene served as the most efficient reducing agent. It was found that the acidity of  $TiO_2$ – $ZrO_2$  is essential for NO reduction by propene on  $In/TiO_2$ – $ZrO_2$ , by the comparison of that on Na-modified  $In/TiO_2$ – $ZrO_2$ . We proposed a reaction pathway on  $In/TiO_2$ – $ZrO_2$  that NO reduction to  $N_2$  proceeds through the reaction of propene and  $NO_2$ , which was formed on the acid sites of  $TiO_2$ – $ZrO_2$ , on the indium sites.

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