# Effect of Pt dispersion on the reduction of NO by propene over alumina-supported Pt catalysts under lean-burn conditions

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Reduction of NO by propene under lean-burn exhaust conditions and oxidation of NO were studied on two  $Pt/\gamma$ - $Al_2O_3$  catalysts of 4.4% and 82% dispersion of Pt. At 265 °C, the turnover frequency for the oxidation of NO was over 100 times higher on the low dispersion than the high dispersion catalyst. The difference was much less pronounced for the reduction of NO. In the reduction of NO, the  $N_2O/N_2$  ratio in the product was found to increase with the conversion of hydrocarbon, while depend much less on Pt dispersion, temperature, or NO conversion.

Keywords: Pt dispersion effect, NO reduction, propene reduction of NO, NO oxidation, NO2 reduction

#### 1. Introduction

The selective reduction of NO with hydrocarbons in the presence of excess oxygen has been studied extensively over the years as a promising method to remove NO from stationary and mobile sources. Although a number of zeolite, metal oxide, and noble metal catalytic systems have been reported to show relatively high catalytic activity for this reaction [1–3], few have been found to satisfy all the requirements for commercial application. Since Pt is the most effective catalyst at low temperatures [4] and resistant toward activity suppression by water [5] and sulfur [6], it appears to be important to understand this catalytic system.

The use of Pt for exhaust gas treatment has been studied extensively for two decades because Pt is a major component in the current automobile exhaust (or three-way) catalysts. However, its catalytic behavior under the exhaust condition of lean-burn gasoline engines has not been studied in detail until recently [7–15]. In laboratory tests, up to about 60% conversion of NO could be achieved. However, substantial amounts of N2O are formed as a product [16]. It has been reported that the selectivity for N<sub>2</sub> or N<sub>2</sub>O depends on the temperature and/or NO conversion [16], and the activity differs depending on whether SiO<sub>2</sub> or Al<sub>2</sub>O<sub>3</sub> is used as support [17] and the nature of the hydrocarbon reductant [14]. There is evidence that the reaction mechanism involves the reaction between adsorbed NO and a surface hydrocarbon species [12,13], instead of, or in addition to NO decomposition and reduction of the oxidized catalyst by hydrocarbon [10]. There is also indication that the NO reduction activity depends on the Pt dispersion; the turnover frequency (TOF) is higher for lower Pt dispersion [16]. This latter finding of the effect of dispersion is similar to that reported for the reduction of NO by H<sub>2</sub> [18]

and the oxidation of propane [19]. Interestingly, the effect of dispersion on CO oxidation varies, depending on the reaction condition ([20] and references therein). Structure sensitivity is also observed in NO reduction by CO on Pd [21] and Rh [22] catalysts.

The purpose of this study is to investigate further the effect of Pt dispersion. In addition to comparing the NO reduction activity, the selectivity for  $N_2$  and  $N_2O$ , and the activity for NO oxidation to  $NO_2$  are also compared on two  $Pt/Al_2O_3$  catalysts of different dispersions. The results of this investigation are reported here.

#### 2. Experimental

Two Pt samples of different Pt dispersions were prepared by the incipient wetness technique using Pt(NH<sub>3</sub>)<sub>2</sub>(NO<sub>2</sub>)<sub>2</sub> dissolved in dilute NH<sub>4</sub>OH. The solution was added to 60–80 mesh  $\gamma$ -alumina (American Cyanamid, BET surface area: 126 m²/g, pore volume: 0.49 cm³/g), which was then dried at 100 °C in air for 40 h. The low Pt dispersion sample was calcined at 400 °C for 3.5 h and reduced in H<sub>2</sub> at 500 °C for 18 h, whereas the high dispersion sample was calcined at 400 °C for 1 h and reduced at 500 °C for 6.5 h. The metal dispersions, as measured by H<sub>2</sub> chemisorption at 298 K using H<sub>2</sub> pulses, were 4.4% and 82%. The metal loading was 0.30% for the low dispersion and 0.27% for the high dispersion sample.

For NO reduction, a 200 ml/min flow of 930 ppm NO, 930 ppm C<sub>3</sub>H<sub>6</sub>, 5% O<sub>2</sub>, 1.6% H<sub>2</sub>O and balance He was passed over a catalyst. Typically, 0.1–0.3 g of the low dispersion catalyst and 0.05–0.15 g of the high dispersion catalyst were used. For NO oxidation, the same feed mixture but without propene or water was used with 0.1 g catalyst at the same total flow rate. For NO<sub>2</sub> reduction, the same feed except with 900 ppm NO<sub>2</sub> and 80 ppm NO instead of

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Table 1
Reduction of NO and propene oxidation over 0.1 g low dispersion Pt/Al<sub>2</sub>O<sub>3</sub> catalyst.

Temp.		C <sub>3</sub> H <sub>6</sub> oxidation				
(°C)	% yield to N <sub>2</sub>	% yield to N <sub>2</sub> O	% yield to NO <sub>2</sub>	% NO conv.	% C <sub>3</sub> H <sub>6</sub> conv.	% C <sub>3</sub> H <sub>6</sub> conv.
265	13.1	3.6	2.6	19.3	26.4	100
275	19.2	14.3	3.5	37.0	74.6	100
285	20.5	18.6	4.0	42.9	100	100
300	16.4	15.9	18.7	51.0	100	100

Table 2 Reduction of NO and propene oxidation over  $0.1~\mathrm{g}$  high dispersion Pt/Al<sub>2</sub>O<sub>3</sub> catalyst.

Temp.		C <sub>3</sub> H <sub>6</sub> oxidation				
(°C)	% yield to N <sub>2</sub>	% yield to N <sub>2</sub> O	% yield to NO <sub>2</sub>	% NO conv.	% C <sub>3</sub> H <sub>6</sub> conv.	% C <sub>3</sub> H <sub>6</sub> conv.
255	12.6	6.9	2.6	22.1	34.3	100
265	18.3	21.4	4.5	44.2	100	100
275	16.8	20.7	5.8	43.3	100	100
285	10.1	18.9	7.0	36.0	100	100

 $\label{eq:Table 3} Table \ 3$  NO oxidation over 0.1 g Pt/Al\_2O\_3 catalysts.

Temp.	% NO conversion				
(°C)	Low Pt dispersion	High Pt dispersion			
255		2.1			
265	39	4.6			
275	47	5.3			
285	51	7.5			
300	57				

NO was used with 0.1 g catalyst at the same total flow rate. The reaction products were monitored with a gas chromatograph using a Porapak Q and a molecular sieve 5A column and  $NO_x$  chemiluminescence analyzer.

## 3. Results and discussion

Tables 1 and 2 show some sample data for the reduction of NO over the two catalysts. From these data, it can be seen that the activities for the two catalysts were similar, with the low dispersion catalyst being somewhat more active. At 245 °C, the TOF for NO conversion was estimated to be 10 min<sup>-1</sup> for the low dispersion sample, and 0.8 min<sup>-1</sup> for the high dispersion sample, using data at 30-40% conversion of propene and about 20% conversion of NO. These values were approximate because they were not obtained under differential conditions. Although similar maximum total NO conversions were achieved by the two catalysts, more N2O was produced than N2 over the high dispersion sample when the propene conversion was close to 100%, whereas the N<sub>2</sub> yield was always higher than the N<sub>2</sub>O yield on the low dispersion sample. This observation differed from the previous report [23], in which metal dispersion did not affect the selectivity toward  $N_2O$ .

On the other hand, the rates of NO oxidation were vastly different over the two catalysts, as shown in table 3, which

agrees with the literature report [9]. At 265 °C, the TOF of the low dispersion sample was >50 min<sup>-1</sup>, compared with 0.3 min<sup>-1</sup> for the high dispersion sample, estimated using relatively high conversion data for the former catalyst. However, although the activity for NO oxidation was much higher for the low dispersion sample, only small amounts of NO<sub>2</sub> were present in the exit gas during NO reduction. Thus, either the presence of hydrocarbon reductant suppresses the NO oxidation activity, or the NO<sub>2</sub> formed is rapidly reduced back to NO. For the high dispersion sample, only small amounts of NO<sub>2</sub> were observed in the exit gas, also consistent with its low activity for NO oxidation.

Reduction of  $NO_2$  by propene was studied, and the results are summarized in table 4. On both catalysts, reduction of  $NO_2$  to NO was very fast, much faster than its reduction to  $N_2$ . This is consistent with the observed low  $NO_2$  concentration in the gas phase during NO reduction. It also implies that NO reduction does not involve first formation of  $NO_2$  followed by its reduction. Interestingly, similar  $N_2/N_2O$  ratios were observed as in NO reduction. This suggests that most likely, the reduction of  $NO_2$  proceeds by its reduction to NO first, which is then reduced to  $N_2$  or  $N_2O$ . Another interesting observation is that the rate of propene conversion was lower than during NO reduction. Probably,  $NO_2$  suppresses the adsorption of  $O_2$  and reduces the rate of propene oxidation. When all the propene is consumed,  $NO_2$  appears in the gas phase again.

The effect of space velocity was studied by varying the amount of catalyst. As expected, using a larger sample lowered the temperature to achieve a certain NO conversion. When the  $N_2$  and  $N_2O$  yields were plotted against propene conversion as shown in figures 1 and 2, a trend is observed that the selectivity for  $N_2O$  appears to be related primarily to the propene conversion, with smaller effect due to temperature, NO conversion, or Pt dispersion. The selectivity for  $N_2O$  increases with propene conversion. This dependence of  $N_2O$  selectivity on propene conversion dif-

 $\label{eq:Table 4} Table \ 4$  Reduction of NO  $_2$  over 0.1 g Pt/Al  $_2O_3$  catalysts.

Temp.	Low Pt dispersion			High Pt dispersion				
(°C)	% NO <sub>2</sub> to N <sub>2</sub>	% NO <sub>2</sub> to N <sub>2</sub> O	% NO <sub>2</sub> to NO	% C <sub>3</sub> H <sub>6</sub> conv.	% NO <sub>2</sub> to N <sub>2</sub>	% NO <sub>2</sub> to N <sub>2</sub> O	% NO <sub>2</sub> to NO	% C <sub>3</sub> H <sub>6</sub> conv.
265					7.2	3.2	94.5	31.1
275	6.2	2.0	94.8	30.5	12.0	15.9	74.6	92.2
285	14.9	15.2	73.8	92.3	14.3	16.4	71.5	100
300	16.8	15.4	43.1	100				

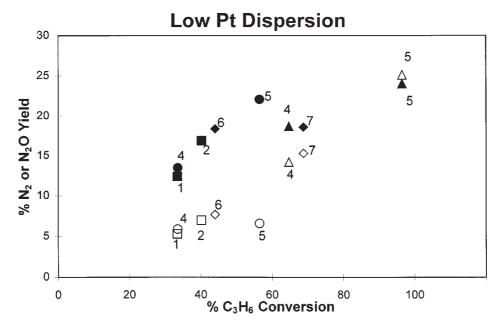


Figure 1. Relationship between propene conversion and yield of  $N_2$  and  $N_2O$  over the low Pt dispersion sample obtained at various space velocities. Catalyst weight: 0.1 g ( $\spadesuit$ ), 0.2 g ( $\bullet$ ), 0.25 g ( $\blacktriangle$ ) and 0.3 g ( $\blacksquare$ ). Closed symbols for  $N_2$  and open symbols for  $N_2O$ . Temperatures in  $^{\circ}C$  are: 240 (1), 245 (2), 250 (3), 255 (4), 265 (5), 275 (6) and 280 (7).

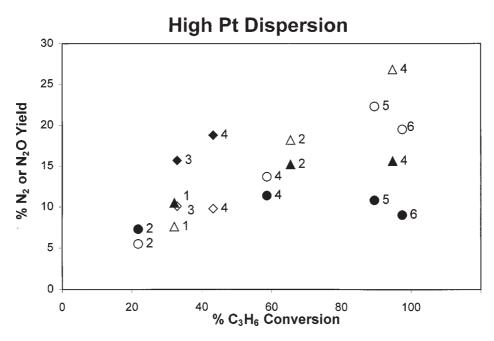


Figure 2. Relationship between propene conversion and yield of  $N_2$  and  $N_2O$  over the high Pt dispersion sample obtained at various space velocities. Catalyst weight: 0.1 g ( $\spadesuit$ ), 0.05 g ( $\bullet$ ) and 0.15 g ( $\blacktriangle$ ). Closed symbols for  $N_2$  and open symbols for  $N_2O$ . Temperatures in  $^{\circ}C$  are: 245 (1), 255 (2), 260 (3), 265 (4), 275 (5) and 285 (6).

fers from the literature result where no dependence was observed [13,18].

The increase in  $N_2O$  selectivity with increasing hydrocarbon conversion agrees with the mechanism of its formation. In the current understanding,  $N_2O$  is formed from molecular adsorption of NO, which is preferred to dissociative adsorption when the density of free surface Pt atoms is low. At low hydrocarbon conversions, the partial pressure of hydrocarbon is high (relatively), correspondingly the surface is covered with a high density of hydrocarbon intermediates, which react with NO to form  $N_2$  [15]. As the hydrocarbon conversion increases, the density of such intermediates decreases, while the fraction of free Pt and oxygen-covered surface increases, which favors the formation of  $N_2O$  [11,14].

It is interesting that the rate of oxidation of NO depends much more strongly on Pt dispersion than NO reduction. The reduction of NO has been proposed to involve a cluster of five or more Pt atoms [18]. Thus, one would expect this process to depend quite strongly on the Pt dispersion. The relatively small effect of Pt dispersion could be due to the fact that the predominant reaction is between adsorbed NO and the surface hydrocarbon species, which would require as little as only adjacent Pt atoms. On the other hand, one would expect the NO oxidation reaction to be similar to CO oxidation. CO oxidation has been shown to occur much faster on a more highly dispersed Pt catalyst at low pressures [20], but the dispersion dependence decreases at high pressures. In the low pressure regime, the kinetics is strongly influenced by the rate of desorption of CO, which is a structure-sensitive process. Perhaps the rate of desorption of NO is also structure-sensitive, and the strong effect of Pt dispersion on NO oxidation is observed at the low pressures of NO used here.

In conclusion, the dependence on Pt dispersion of NO oxidation and propene reduction of NO was studied. The turnover rate of NO oxidation to  $NO_2$  depends strongly on the Pt dispersion. The dependence is much weaker for the reduction of NO. Thus, the reduction of NO does not involve NO oxidation to  $NO_2$ . In the reduction of NO, the  $N_2O/N_2$  ratio in the product depends much more strongly on the conversion of hydrocarbon than Pt dispersion, temper-

ature, or NO conversion. The latter result can be explained by the mechanism that the formation of  $N_2O$  is favored on an oxygen-covered surface, and  $N_2$  is formed on a surface covered with hydrocarbon intermediates.

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