# Partial oxidation of methane to synthesis gas over Ru-loaded $Y_2O_3$ catalyst

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Ru-loaded  $Y_2O_3$  catalyst was investigated for the partial oxidation of methane to synthesis gas. Ru(0.5 wt%)/ $Y_2O_3$  catalyst afforded a high CH<sub>4</sub> conversion of 27% at a CH<sub>4</sub>:  $O_2$  ratio of 5 to give nearly a 1:2 ratio of CO and H<sub>2</sub> with a selectivity of 75% at 873 K. Ru(0.5 wt%)/ $Y_2O_3$  catalyst maintained high catalytic activity over 10 h in the partial oxidation of methane. Carbon deposition of the catalyst surface in the reaction of CH<sub>4</sub> was examined by thermogravimetric analyses, and it was found that no carbon deposition occurred on the Ru(0.5 wt%)/ $Y_2O_3$  catalyst. The synthesis-gas production proceeded basically *via* a two-step reaction consisting of methane combustion to give H<sub>2</sub>O and CO<sub>2</sub>, followed by the reforming of methane from CO<sub>2</sub> and steam.

KEY WORDS: methane; thermogravimetric; carbon deposition.

#### 1. Introduction

Recently, natural gas has been given much attention as a fossil fuel resource. Due to its high hydrogen:carbon ratio, natural gas is able to mitigate  $CO_2$  emission. Although its use as fuel is of interest, its use as a hydrogen source for fuel cells is an additional important aspect of natural gas. In order to convert the natural gas into raw material for chemical reactions, conversion of natural gas into synthesis gas  $(H_2, CO)$  must first be accomplished by reforming reactions using  $H_2O$  (reaction 1) or  $CO_2$  (reaction 2), and also a partial oxidation reaction (reaction 3). The three reactions proceed as follows.

The steam reforming reaction of methane

$$\mathrm{CH_4} + \mathrm{H_2O} \rightleftharpoons \mathrm{CO} + 3\mathrm{H_2} \qquad \Delta H_{298}^{\mathrm{o}} = +206\,\mathrm{kJ/mol}.$$

(1)

The CO<sub>2</sub> reforming reaction of methane

$$CH_4 + CO_2 \rightleftharpoons 2CO + 2H_2$$
  $\Delta H_{298}^o = +247 \text{ kJ/mol.}$ 

The partial oxidation reaction of methane

$$\label{eq:charge_energy} CH_4 + \tfrac{1}{2}O_2 \rightarrow CO + 2H_2 \qquad \Delta \textit{H}_{298}^o = -36\,\text{kJ/mol}.$$

(3)

Steam reforming is an industrially established process for converting natural gas into synthesis gas; highly efficient plants have been constructed, but with large investment costs. The partial oxidation of methane is an exothermic reaction. Recently, this reaction has been re-examined from the viewpoint of saving energy. A characteristic feature of this reaction is to obtain synthesis gas with a  $H_2/CO$  ratio of 2. This ratio is adequate for methanol synthesis or for synthesis of higher hydrocarbons by the Fischer–Tropsch reaction. One of the major problems involved in the commercialization of this process is to avoid carbon deposition during the partial oxidation of methane. In addition, the high cost of an oxygen plant is a hindrance to commercialization.

The group VIII transition elements of noble metals (Ru, Rh, Ir, Pt, Pd) and non-noble metals (Co, Ni, Fe) have been reported as active catalysts for the partial oxidation of methane. We have reported that Ir/TiO<sub>2</sub> showed high activity without carbon deposition for the partial oxidation of methane [1-3]. Dissanayake et al. [4] carried out the partial oxidation of methane over a Ni/A1<sub>2</sub>O<sub>3</sub> catalyst and obtained high selectivities of the synthesis gas. NiO/MgO solid solution catalyst [5] and LiLaNiO/\gamma-Al2O3 catalyst [6] were reported to be active catalysts for the partial oxidation of methane. Hickman and Schmidt [7] investigated A12O3 monolith-supported Rh and Pt catalysts for the partial oxidation of methane. It has also been reported that the Rh/MgO catalyst was a highly active and selective catalyst in the partial oxidation of methane [8].

Noble metals are too expensive for large-scale commercial use. However, Ru and Rh have been shown to be carbon resistant, whereas non-noble metals are prone to deactivation by coke [9,10]. Although Rh is a highly active metal, it is one of the most expensive materials that can be used as a catalyst. Therefore, we focused on the less expensive Ru as a catalyst.

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Studies have already been published on the partial oxidation of methane with a Ru-loaded catalyst. Ashcroft et al. [11] reported that CO and H<sub>2</sub> are obtained from CH<sub>4</sub> and O<sub>2</sub> at 1050 K by using Ln<sub>2</sub>RuO<sub>7</sub> (Ln = lanthanide) catalyst with high yield and high selectivity. Poirier et al. [12] examined the same reaction by using Ru/Al<sub>2</sub>O<sub>3</sub> as a catalyst, while Moffat and Matsumura [13] employed the Ru/SiO<sub>2</sub> catalyst. Partial oxidation of methane is believed to proceed in two steps, as shown in reactions (4), (1), and (2) [2].

$${
m CH_4 + 2O_2 \to CO_2 + 2H_2O} \qquad \Delta H_{298}^{\rm o} = -801\,{\rm kJ/mol.}$$
 (4)

We have carried out the  $CO_2$  reforming of methane with the  $Ru/La_2O_3$  catalyst. In the course of  $CO_2$  reforming (reaction (2)), several lanthanoid-loaded Ru catalysts afforded high activity for the partial oxidation of methane [14]. Thus,  $Ru/Ln_2O_3$  catalysts are candidates as an active catalyst for the partial oxidation of methane. In this paper, we consider  $Ru/Ln_2O_3$  catalysts for the partial oxidation of methane. In particular, we focus on detailed studies of the  $Ru/Y_2O_3$  catalyst, in which active and stable oxide forms have been obtained.

#### 2. Experimental

### 2.1. Catalyst preparation

The catalyst supports used in the present study were  $Al_2O_3$  (JRC-ALO-4),  $SiO_2$  (Merck), MgO (500A; Ube Industries, Ltd.),  $TiO_2$  (P25; Japan Aerosil Co.),  $Sm_2O_3$ ,  $Eu_2O_3$  (Anan Chemicals),  $Pr_6O_{11}$  (Santoku Metal Industry),  $Nd_2O_3$  (Nacalai Tesque, Inc.), CaO (Wako Pure Chemical Industry),  $Y_2O_3$ -stabilized  $ZrO_2$  (Strem Chemicals),  $Y_2O_3$ ,  $La_2O_3$ ,  $CeO_2$ , and  $ZrO_2$ . The catalyst supports of  $Y_2O_3$ ,  $La_2O_3$ ,  $CeO_2$ , and  $ZrO_2$  were prepared by the thermal decomposition of  $Y_2(C_2O_4)_3 \cdot ^4H_2O$ ,  $La(CH_3COO)_3 \cdot ^3_2H_2O$ ,  $Ce(NO_3)_3 \cdot ^3_2H_2O$ , and  $ZrO_2 \cdot ^nH_2O$  (Wako Pure Chemical Industry) at 873 K in air at atmospheric pressure for 5 h.

Group VIII metal-loaded catalysts were prepared by impregnating an aqueous solution of RuCl<sub>3</sub>·nH<sub>2</sub>O, Pd(CH<sub>3</sub>COO)<sub>2</sub>, IrCl<sub>4</sub>·H<sub>2</sub>O, (NH<sub>3</sub>)<sub>2</sub>Pt(NO<sub>2</sub>)<sub>2</sub>, Co-(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, RhCl<sub>3</sub>·H<sub>2</sub>O (Mitsuwa Pure Chemicals), Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O, Ni(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (Wako Pure Chemical Industry) onto metal oxides. Water was removed by evaporation under reduced pressure. Dried catalysts were calcined at 873 K in air for 5 h.

#### 2.2. Catalytic reaction

The reaction was carried out with a fixed-bed flow-type quartz reactor (i.d.  $8 \times 350 \,\mathrm{mm}$ ) at atmospheric pressure. Using 60 mg of catalyst, 25 ml/min of CH<sub>4</sub> and 5 ml/min of O<sub>2</sub> were introduced at a temperature

range of 673-973 K. Before the reaction, the catalysts were reduced with  $H_2$  for 1 h at 873 K with a heating rate of 30 K/min from room temperature. Products were analyzed with an online high-speed gas chromatograph (PC-Chrom, M200 Chromato Analyzer).

#### 2.3. Characterization

X-ray photoelectron spectra (XPS) of the catalyst were obtained on a Jeol model JPS-9000MX using Mg  $K_{\alpha}$  radiation as the energy source.

Carbon deposition behavior was achieved by using a thermogravimetric analyzer (Shimadzu, TGA-50). A 13 mg sample was placed on the TG pan. Heating was programmed at a rate of  $20 \, \text{K/min}$  to a prescribed temperature under an Ar atmosphere. After reaching the desired temperature, the Ar flow was switched to a  $\text{CH}_4$ -air ( $\text{CH}_4$  = 15, air = 15 ml/min) mixture, and the catalyst weight increase in the sample was monitored.

Transient response measurement of the catalyst bed temperature in the pulsed reactions was carried out using a fixed-bed quartz reactor (i.d.  $4\,\mathrm{mm} \times 200\,\mathrm{mm}$ ). In the front edge of the catalyst bed, thin wall sheathed thermocouples were set and  $100\,\mathrm{mg}$  of the catalyst was charged. A pulse of CH<sub>4</sub> and O<sub>2</sub> (2:1) mixed gas was introduced with a six-port gas-sampling valve equipped with measuring tubes, under a steam of Ar carrier gas [3,19]. Before the reaction, the catalysts were reduced under H<sub>2</sub> flow for 1 h at 873 K.

The reaction temperature was controlled by monitoring the outside temperature of the reactor wall by using a programmable controller. Analyses of the gases during the methane decomposition were made using an online quadrupole mass spectrometer (HAL201, Hiden Analytical Ltd.). The mass spectrometer scanned the parent peaks of the five compounds (H<sub>2</sub>, CO, CO<sub>2</sub>, O<sub>2</sub> and CH<sub>4</sub>) within 1 s, and repeated scans were collected in a personal computer.

### 3. Results and discussion

# 3.1. Effect of support on the activity of Ru-loaded catalysts

Table 1 shows the specific surface area of the catalysts and the conversion of methane as well as CO, CO<sub>2</sub> and H<sub>2</sub> selectivities in the partial oxidation of methane over Ru(0.5 wt%) loaded catalysts. The order of the catalytic activity in the different supports at 873 K was La<sub>2</sub>O<sub>3</sub> >  $Y_2O_3 > CeO_2 > ZrO_2 > SiO_2 > TiO_2 > Al_2O_3 > Pr_6O_{11} > Nd_2O_3 > Sm_2O_3 > Eu_2O_3 > MgO > YSZ > CaO$ . When La<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> were used for support, these catalysts afforded high CH<sub>4</sub> conversion into CO and H<sub>2</sub> with selectivities of over 75% and a H<sub>2</sub>:CO ratio of 2, as was expected from the stoichiometry of the reaction (reaction (3)). On these supports, higher CH<sub>4</sub> conversions were obtained than those observed in studies

Catalyst	Surface area $(m^2/g)$	Conversion (%) CH <sub>4</sub>	Selectivity (%)			H <sub>2</sub> /CO
			СО	CO <sub>2</sub>	H <sub>2</sub>	(ratio)
Ru/La <sub>2</sub> O <sub>3</sub>	19.1	29.0	79.9	20.1	78.9	2.0
$Ru/Y_2O_3$	13.7	27.5	78.9	21.1	79.2	2.0
Ru/CeO <sub>2</sub>	70.2	27.3	81.7	18.3	79.5	2.0
$Ru/ZrO_2$	40.0	23.5	79.8	20.2	82.1	2.1
Ru/SiO <sub>2</sub>	399	16.5	59.9	40.4	76.8	2.6
Ru/TiO <sub>2</sub>	37.8	15.9	72.3	27.7	61.8	1.7
$Ru/Al_2O_3$	176	14.3	62.4	37.6	63.9	2.1
$Ru/Pr_6O_{11}$	1.7	10.1	8.6	91.4	23.9	5.6
$Ru/Nd_2O_3$	3.3	9.7	12.0	88.0	19.5	3.4
$Ru/Sm_2O_3$	4.6	9.4	8.1	91.9	19.1	4.6
$Ru/Eu_2O_3$	8.1	7.6	37.9	62.1	_	_
Ru/MgO	37.4	3.6	15.0	85.0	3.9	0.6
Ru/YSZ	n.d.	1.6	_	100	_	_
Ru/CaO	11.5	_	_	_	_	_

Table 1
Activity of supported Ru(0.5 wt%) catalysts for the partial oxidation of methane

Note: Catalyst: 60 mg. Flow rate: 30 ml/min (CH<sub>4</sub>/O<sub>2</sub> = 5). Reaction temperature: 873 K. n.d.: not determined.

of Ru supported on  $Al_2O_3$  or  $SiO_2$  catalyst. If the partial oxidation of methane (reaction (3)) was assumed to be the main reaction path of synthesis-gas production,  $CH_4$  conversion would be expected to be limited to 40%, due to the smaller  $CH_4:O_2$  ratio (5:1). Complete oxidation (reaction (4)) gave a  $CH_4$  conversion of 10%. The characteristic feature of  $Ru/Pr_6O_{11}$ ,  $Ru/Nd_2O_3$  and  $Ru/Sm_2O_3$  is the high catalytic activity, affording the complete oxidation of methane (reaction (4)) and  $CO_2$  as a major product.

In the case of  $CO_2$  reforming of methane using the  $La_2O_3$ -supported catalyst, catalytic activity varied considerably during the reaction, and  $La_2O_3$  was transformed into  $La_2O_2\cdot CO_3$  or  $La(OH)_3$ . Thus, the  $La_2O_3$ -supported catalyst showed changes in structure during the reaction, as has been described previously in the case of  $CO_2$  reforming [14]. To avoid such changes in the support structure, further studies were carried out using a  $Y_2O_3$ -supported catalyst.

# 3.2. Effect of the Ru loading level on the partial oxidation of methane

The effect of the Ru loading level on the partial oxidation of methane using  $Ru/Y_2O_3$  catalyst is shown in figure 1. The reaction occurred with a loading level as low as 0.1 wt%, and  $\sim\!25\%$  CH<sub>4</sub> conversion and a synthesis gas selectivity of  $\sim\!70\%$  were obtained with a loading level of 0.5 wt%. Further increases in the loading level to 5 wt% only slightly increased CH<sub>4</sub> conversion, to 30%.

# 3.3. Effect of reaction temperature of $Ru/Y_2O_3$ catalyst on the partial oxidation of methane

Figure 2 shows the temperature dependence of the partial oxidation of methane over Ru(0.5 wt%)/Y<sub>2</sub>O<sub>3</sub>

catalyst. The reaction did not proceed at 673 K, and methane conversion occurred above 773 K. The amounts of CO and H<sub>2</sub> increased and the amount of CO<sub>2</sub> decreased with increasing reaction temperatures. At 973 K, Ru(0.5 wt%)/Y<sub>2</sub>O<sub>3</sub> catalyst afforded a methane conversion of 35%. The ratio of H<sub>2</sub> to CO at 973 K decreased to less than 2. The reason for this effect seems to be a reverse water–gas shift reaction (5), where H<sub>2</sub> was consumed to give CO and H<sub>2</sub>O. It seems reasonable to assume that the reaction proceeded favorably at a higher temperature due to the endothermic nature of the reaction.

$$H_2 + CO_2 \rightleftharpoons CO + H_2O$$
  $\Delta H_{298}^o = +41 \text{ kJ/mol.}$  (5)

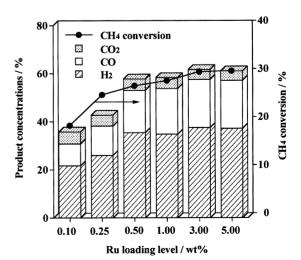


Figure 1. Effect of Ru-loading level of  $Y_2O_3$  catalyst on the partial oxidation of methane. Flow rate:  $30\,\text{ml/min}$  (CH<sub>4</sub>/O<sub>2</sub> = 5). Reaction temperature: 873 K. Catalyst: 60 mg.

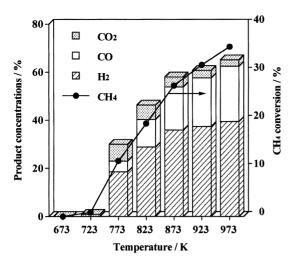


Figure 2. Effect of temperature on the  $CH_4$  conversion and product concentrations over  $Ru/Y_2O_3.$  Flow rate:  $30\,ml/min$  ( $CH_4/O_2=5$ ).  $SV=30\,000\,h^{-1}$  ml/g-catalyst. Catalyst:  $60\,mg.$ 

### 3.4. Active form of ruthenium in the $Ru/Y_2O_3$ catalyst

In order to determine the characteristics of the ruthenium species on Y<sub>2</sub>O<sub>3</sub>, the fresh and the used catalysts were examined with XPS, and the results are shown in figure 3. The fresh calcined Ru/Y<sub>2</sub>O<sub>3</sub> catalyst showed two peaks at 464.0 and 462.8 eV, which were ascribed to Ru(IV)O<sub>2</sub> and Ru(II)O (a), respectively, since the catalyst was prepared by calcination under air flow at 873 K. When the catalyst was reduced with hydrogen at 873 K for 1 h (f), the strong peak shifted to a lower binding energy, indicating that oxidic ruthenium was reduced to metallic ruthenium. After the reaction at 723 K for 2 h, the catalyst was subjected to XPS analysis: the spectrum is shown in (b). Before the reaction, the Ru/ Y<sub>2</sub>O<sub>3</sub> catalyst was reduced under H<sub>2</sub> flow for 1 h at 873 K, and the reduced catalyst was used for the reaction at 723 K. After the reaction, the used catalyst was subjected to XPS analysis (c). Peaks at 462.8 eV of RuO observed in the spectrum shown in (a) shifted to 462.4 eV (b) and 462.2 eV (c), and almost the same spectra as those observed on (b) and (c) were obtained. It appears that RuO was reduced slightly. Although RuO (c) was reduced to Ru metal by H<sub>2</sub> reduction, Ru metal was oxidized again under the CH<sub>4</sub>-O<sub>2</sub> flow. The observed peak at 464.0 eV (a) of RuO<sub>2</sub> did not alter the reaction (spectrum (b) and spectrum (c)). The partial oxidation reaction did not proceed at 723 K using both reduced Ru/Y<sub>2</sub>O<sub>3</sub> and unreduced Ru/Y<sub>2</sub>O<sub>3</sub> catalysts. These results demonstrate that only RuO of the Ru/Y<sub>2</sub>O<sub>3</sub> catalyst was reduced at 723 K. The partial oxidation of methane did not proceed, even when only RuO was reduced.

After the reaction at 873 K, the  $Ru/Y_2O_3$  catalyst was subjected to XPS (d). Again prior to the reaction, the  $Ru/Y_2O_3$  catalyst had been reduced under  $H_2$  flow for 1 h at 873 K, and the catalyst after the reaction at 873 K for 2 h

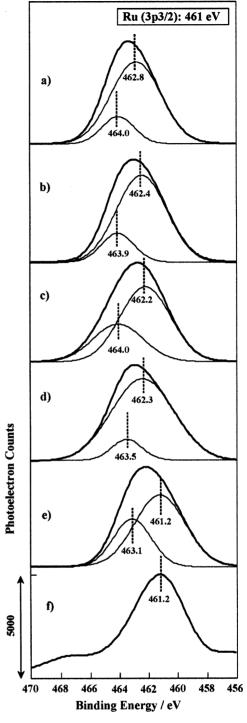


Figure 3. XPS spectra of  $Ru(3p_{3/2})$  on  $Ru/Y_2O_3$  catalyst. (a) Fresh catalyst. (b) Catalyst after the reaction with  $CH_4/O_2$  at 723 K for 2 h. (c)  $H_2$  reduced catalyst after the reaction with  $CH_4/O_2$  at 723 K for 2 h. (d) Catalyst after the reaction with  $CH_4/O_2$  at 873 K for 2 h. (e)  $H_2$  reduced catalyst after the reaction with  $CH_4/O_2$  at 873 K for 2 h. (f)  $H_2$  reduced catalyst at 873 K for 1 h.

was subjected to XPS analysis; the spectrum is shown in (e). At 873 K, the Ru-supported Y<sub>2</sub>O<sub>3</sub> catalyst produced synthesis gas for the partial oxidation of methane. Peaks at 464.0 eV and 462.8 eV of the oxidic form (a) shifted slightly to a lower binding energy side of 463.5 eV and

462.3 eV (d). The results shown in spectrum (d) indicate that both RuO and RuO<sub>2</sub> were reduced slightly. Peaks at 464.0 eV and 462.8 eV of the oxidic form observed in spectrum (a) shifted to 463.1 = eV and 461.2 eV (e). It appears that RuO<sub>2</sub> was reduced slightly to a lower valency state of oxides, and RuO was reduced to metallic ruthenium. When both RuO and RuO<sub>2</sub> were reduced, the synthesis gas was produced. Active species of the Ru/Y<sub>2</sub>O<sub>3</sub> catalyst appear to be species observed in spectra (d) and (e). These results clearly show that the active species of the Ru/Y<sub>2</sub>O<sub>3</sub> catalyst for the partial oxidation of methane to synthesis gas were in the reduced RuO and in the reduced forms of RuO<sub>2</sub>.

The XRD pattern of fresh catalyst showed diffraction peaks assignable to  $RuO_2$ . In a previous paper [15], we elucidated that  $Ru/La_2O_3$  catalyst afforded both  $RuO_2$  and metallic Ru after  $CO_2$  reforming of methane.

# 3.5. Effect of group VIII metal on the performance of the partial oxidation of methane

Figure 4 shows CH<sub>4</sub> conversion and product distribution in the partial oxidation of group VIII metal (0.5 wt%) supported Y<sub>2</sub>O<sub>3</sub> catalysts. The order of the catalytic activity of the group VIII transition metals loaded on Y<sub>2</sub>O<sub>3</sub> in the partial oxidation of methane was unusual. CH<sub>4</sub> conversion and selectivities to CO and  $H_2$  were the highest with the  $Ru/Y_2O_3$  catalyst. Although just above Ru in the periodic table, Fe did not show activity. Co and Rh did not show activity, but Ir exhibited high activity. Choudhary et al. [16] reported that metallic cobalt or partially reduced CoO dispersed on the rare earth oxide seemed to be active phases of partial oxidation. However, Co supported on Y<sub>2</sub>O<sub>3</sub> catalyst did not produce synthesis gas, and even the hydrogen-treated Co/Y2O3 did not afford synthesis gas. These results seem to suggest that Co<sub>2</sub>O<sub>3</sub> or CoO,

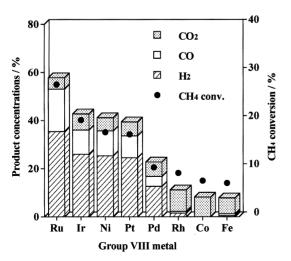


Figure 4. Partial oxidation of methane over  $Y_2O_3$ -supported transition metals. Flow rate:  $30\,\text{ml/min}$  (CH<sub>4</sub>/O<sub>2</sub> = 5). Reaction temperature: 873 K. Catalyst:  $60\,\text{mg}$ .

Table 2 Thermogravimetric analyses of  $Y_2O_3$ -supported catalysts for  $CH_4$  decomposition at 873 K  $^a$ 

Catalyst	Carbon deposition rate	Carbon deposition	
	C μmol/g-cat./min	C μmol	
Ni/Y <sub>2</sub> O <sub>3</sub>	108.7	84.8	
$Rh/Y_2O_3$	34.9	27.3	
Pd/Y <sub>2</sub> O <sub>3</sub>	25.1	19.6	
$Ru/Y_2O_3$	n.d.	n.d.	
$Ir/Y_2O_3$	n.d.	n.d.	
Co/Y2O3	n.d.	n.d.	
$Pt/Y_2O_3$	n.d.	n.d.	
Fe/Y <sub>2</sub> O <sub>3</sub>	n.d.	n.d.	

<sup>&</sup>lt;sup>a</sup> Prior to the reaction, catalysts were reduced with H<sub>2</sub> at 873 K for 1 h. Flow rate = 15 ml/min (CH<sub>4</sub>/air = 1). Reaction time: 1 h. n.d.: not determined.

when on  $Y_2O_3$ , cannot be reduced to metallic cobalt under  $H_2$  at 873 K. Only the lowest of the transition elements, Ni, showed high catalytic activity. Pd and Pt, the 2nd and 3rd lowest elements, exhibited moderate activity. These findings cannot be presented here.

Ni, Rh and Pd catalysts showed gradual deactivation during the partial oxidation reaction. Carbon deposition on group VIII (Ni, Ru, Rh, Pd, Ir, Pt, Fe, Co) metalloaded Y<sub>2</sub>O<sub>3</sub> catalysts were measured under an isothermal reaction at 873 K using a thermogravimetric analysis; the results are shown in table 2. Carbon deposition was not detected with Ru, Ir, Pt, Fe and Co catalysts in reaction with CH<sub>4</sub> for 1 h. In contrast, rapid carbon deposition occurred on Ni, Rh and Pd catalysts in the initial stage of the reaction, indicating that these catalysts would be deactivated by carbon deposition.

### 3.6. Stability of the $Ru/Y_2O_3$ catalyst

Figure 5 shows the effect of time-on-stream on the partial oxidation of methane at 873 K over Ru(0.5 wt%)/ $Y_2O_3$  and Ni/ $Y_2O_3$  catalysts. The Ru(0.5 wt%)/ $Y_2O_3$  catalyst maintained initial catalytic activity for 10 h with a high CH<sub>4</sub> conversion of about 28%. On the other hand, the Ni/ $Y_2O_3$  catalyst showed gradual deactivation over a period of 10 h and carbon deposition was observed after the reaction. The details of the carbon deposition are described in the following section. The problem with using Ni catalysts is formation of whisker carbon deposition on the catalysts, which may lead to plugging of the reformer tubes.

# 3.7. Comparison of $Ru/Y_2O_3$ and Rb catalysts in the partial oxidation of methane

It has been reported that  $Rh/A1_2O_3$  catalyst exhibits high activity in the partial oxidation of methane [17,18]. The differences between several Rh catalysts and  $Ru/Y_2O_3$  catalyst are compared in figure 6. The  $Ru/Y_2O_3$  catalyst showed the same activity as  $Rh/A1_2O_3$ ,

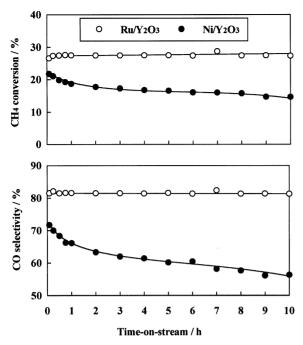


Figure 5. Effect of time-on-stream on the conversion of methane and CO selectivity over  $Ru/Y_2O_3$  and  $Ni/Y_2O_3$  catalysts. Flow rate:  $30 \, ml/min$  ( $CH_4/O_2=5$ ). Reaction temperature:  $873 \, K$ . Catalyst:  $60 \, mg$ .

the activity of which was higher than that of both Rh/TiO<sub>2</sub> and Rh/SiO<sub>2</sub>. However, the Rh catalysts showed carbon deposition after 2 h of reaction. The Ru/Y<sub>2</sub>O<sub>3</sub> catalyst was highly active, without carbon deposition, in the partial oxidation of methane. These results seem to suggest Ru/Y<sub>2</sub>O<sub>3</sub> as an excellent catalyst.

### 3.8. Reaction mechanism of $Ru/Y_2O_3$ catalyst

In order to obtain more detailed information on the reaction pathways of synthesis-gas production over  $Ru/Y_2O_3$  catalyst, the space velocity was varied by

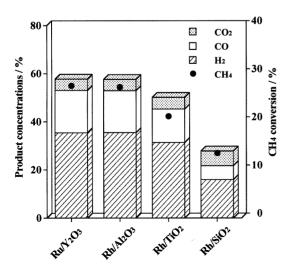


Figure 6. Activity of  $Ru/Y_2O_3$  and various Rb catalysts for the partial oxidation of methane. Flow rate:  $30\,\mathrm{ml/min}$  (CH<sub>4</sub>/O<sub>2</sub> = 5). Reaction temperature:  $873\,\mathrm{K}$ . Catalyst:  $60\,\mathrm{mg}$ .

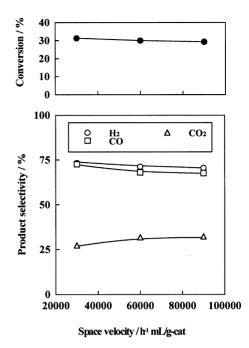


Figure 7. Effect of space velocity on the  $CH_4$  conversion and product selectivities over  $Ru(0.5\,wt\%)/Y_2O_3$ . Flow rate:  $30\,ml/min~(CH_4/O_2=5)$ . Reaction temperature:  $873\,K$ . Catalyst:  $60\,mg$ .

increasing the feed rate at a reaction temperature of  $873 \,\mathrm{K}$ . Figure 7 shows  $\mathrm{CH_4}$  conversion and selectivies to  $\mathrm{CO}$ ,  $\mathrm{H_2}$  and  $\mathrm{CO_2}$  as a function of space velocity, but the  $\mathrm{H_2O}$  selectivity was not determined. The  $\mathrm{CH_4}$  conversion and the  $\mathrm{CO}$  and  $\mathrm{H_2}$  selectivities decreased with increasing space velocity. On the other hand, the  $\mathrm{CO_2}$  selectivity increased. These results seem to support the two-step reaction mechanism, that the  $\mathrm{Ru/Y_2O_3}$  catalyst might have promoted the reaction sequence of total oxidation of methane to  $\mathrm{CO_2}$  and  $\mathrm{H_2O}$  (reaction (4)), and the reforming reactions to synthesis gas (reactions (1), (2)) [2]. If the partial oxidation of methane to synthesis gas is a one-step process (reaction (3)), then the  $\mathrm{CH_4}$  conversion would decrease without changing the  $\mathrm{H_2/CO}$  ratio.

Moreover, in order to investigate the reaction pathways over the  $Ru/Y_2O_3$  catalyst, a pulsed reaction technique was employed to measure transient temperature changes in the catalyst bed [3,19]. Among the four reactions, (1) and (2) were highly endothermic, (3) was moderately exothermic, and (4) was highly exothermic. In this reaction feature, observation of the catalyst bed temperature by means of injecting a pulse of reactants may provide information about the initial reaction that takes place at the catalyst bed [3,19].

Figure 8 shows the transient temperature responses of  $Ru/Y_2O_3$  catalyst against a pulsed injection of  $CH_4/O_2$  (2:1). A sudden rise in the temperature at the front edge of the catalyst bed was observed upon introduction of the pulse of the  $CH_4$  and  $O_2$  mixture (2:1) at 873 K. The temperature increase at the front edge of the catalyst bed could reasonably be ascribed to the exothermic

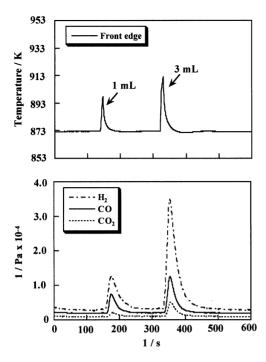


Figure 8. Temperature profile at the front edge of catalyst bed and partial pressure variations with time of the fragments over  $Ru(0.5\,wt\%)/Y_2O_3$  catalyst. Reaction conditions: Ar carrier = 10 ml/min. Mixed gas:  $CH_4/O_2=2$  (1 ml or 3 ml). Furnace temperature: 873 K.

complete oxidation reaction, since the absolute amounts of the increase in temperature are much larger than those observed for the temperature drop in reaction (2). It seems that  $CO_2$  is produced by the complete oxidation reaction (4). The synthesis gas was formed *via* a two-step reaction pathway using the  $Ru/Y_2O_3$  catalyst in this  $CH_4-O_2$  reaction.

### 4. Conclusions

In the case of the  $Ru/Y_2O_3$  catalyst, a low loading level of Ru(0.5 wt%) on  $Y_2O_3$  exhibited very high catalytic activity for the partial oxidation of methane to synthesis gas at 873 K. Moreover, a synthesis gas ratio of  $H_2/CO = 2$  was obtained, and the initial activity was maintained in a 10 h reaction. It is thought that the synthesis-gas production *via* the partial oxidation of

methane proceeded basically by means of a two-step path consisting first of complete oxidation to give  $CO_2$  and  $H_2O$ , followed by the methane reforming with both  $CO_2$  and  $H_2O$ .

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