

# Kinetics of selective oxidation of dimethyl ether to formaldehyde over $\text{Al}_2\text{O}_3$ -supported $\text{VO}_x$ and $\text{MoO}_x$ catalysts

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The kinetic behaviors of dimethyl ether (DME) selective oxidation to formaldehyde were investigated over  $\text{Al}_2\text{O}_3$ -supported  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts. It was shown that the reaction is pseudo-zero order with respect to both dimethyl ether and oxygen molecule, suggesting that the reaction of surface intermediate  $\text{CH}_3\text{O}^*$  is likely to be the rate-determining step. The apparent activation energies for the target reaction were determined to be 122 kJ/mol over the  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst and 125 kJ/mol over the  $\text{MoO}_x/\text{Al}_2\text{O}_3$  catalyst, respectively. With the decrease of contact time, the dimethyl ether conversion decreased linearly, while the selectivity of HCHO increased, indicating that formaldehyde is the preliminary product of the selective oxidation of dimethyl ether.

**KEY WORDS:** dimethyl ether; selective oxidation; formaldehyde; kinetics; supported  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts.

## 1. Introduction

Compared with methanol synthesis from synthesis gas, the similar process of dimethyl ether (DME) production from the same feed provides more economically attractive advantages by breaking the thermodynamic restriction, which lead to higher single-pass CO conversion [1]. These great economical potential and environmental benign features of this process make DME an attractive raw material for replacing methanol to produce formaldehyde, acetic acid, and olefins, etc. [2–3], and consequently, lead to the emergence of DME catalytic reaction chemistry. As a matter of fact, the surface methoxide intermediate ( $\text{CH}_3\text{O}$ ) involved in methanol reactions can also be generated by the cleavage of the  $\text{CH}_3\text{OCH}_3$  molecule over metal oxide catalysts under mild reaction conditions [4].

Particularly, the selective oxidation of DME to formaldehyde (HCHO) has attracted much attention in recent years [3].  $\text{MoO}_x$  and  $\text{VO}_x$  supported on  $\text{Al}_2\text{O}_3$ ,  $\text{ZrO}_2$  and  $\text{SnO}_2$  were reported to be reactive for DME selective oxidation to formaldehyde around 550 K, which is much lower than the required temperature of conventional production of formaldehyde via oxidative dehydrogenation of methanol on iron molybdates or Ag-based catalysts [5–6]. Both the conversion of DME and the selectivity to HCHO increased with the  $\text{MoO}_x$  or  $\text{VO}_x$  surface density up to their monolayer dispersion capacities [7–9]. Raman and X-ray absorption spectroscopies were used to probe the structure of the  $\text{MoO}_x$  domains with the observation that the  $\text{MoO}_x$  domain surfaces become more active as two-dimensional monolayers

formed through oligomerization of monomer  $\text{MoO}_x$  species. Meanwhile, the redox properties of  $\text{MoO}_x$  domains also influence DME reaction [7]. The initial  $\text{H}_2$  reduction rate of the  $\text{MoO}_x$  species related to the C–H bond activation of the  $\text{CH}_3\text{O}^*$  intermediate was linearly correlated with the DME reaction rate [9]. Modification of the  $\text{Al}_2\text{O}_3$  support with reducible oxides, which made the  $\text{MoO}_x$  domains more reducible, led to higher DME reaction rates, while maintaining the HCHO selectivity nearly constant [10]. It is generally accepted that the two-dimensional monolayer  $\text{MoO}_x$  is more active for the dehydrogenation of adsorbed methoxide species by lattice oxygen, which is regarded as the rate-determining step of DME oxidation. However, most of the previous studies were focused on  $\text{MoO}_x$  catalysts, and only few investigations have been conducted on  $\text{VO}_x$  catalysts. Our recent studies showed that  $\text{Al}_2\text{O}_3$  supported  $\text{VO}_x$  catalysts even gave better catalytic activities than that of  $\text{MoO}_x$  catalysts, e.g., lower reaction temperatures could be applied to obtain the same DME conversion over supported  $\text{VO}_x$  catalyst [8].

In this work, kinetic studies on the selective oxidation of DME to HCHO over  $\text{Al}_2\text{O}_3$  supported  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts were carried out with the aim to establish the reaction kinetic models and to explore the detailed reaction mechanism.

## 2. Experimental

### 2.1. Catalyst preparation

A commercially available  $\gamma\text{-Al}_2\text{O}_3$  with a BET surface area of 227  $\text{m}^2/\text{g}$  was used to load  $\text{V}_2\text{O}_5$  by the wet-impregnation method, in which the desirable amount of ammonium metavanadate (18% of  $\text{V}_2\text{O}_5$  by weight

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with respect to the final catalyst) was dissolved in 0.4 M oxalic acid solution at a molar ratio of  $V : H_2C_2O_4 = 2 : 1$ . The excess water was then evaporated at 323 K. A 30 wt%  $MoO_3/Al_2O_3$  catalyst, having the same amount of active metal atoms as that of 18 wt%  $V_2O_5/Al_2O_3$ , was prepared by the incipient wetness impregnation of the  $\gamma$ - $Al_2O_3$  with an aqueous ammonium heptamolybdate  $((NH_4)_6Mo_7O_{24} \cdot 4H_2O)$  solution. Both samples obtained were dried at 373 K overnight and then calcined at 773 K for 3 h in air. The catalysts were pressed, crushed, and sieved to 40–60 meshes for reaction test.

## 2.2. Catalysts characterization

### 2.2.1. Surface area

Surface areas were measured by nitrogen adsorption at 97 K using a Micrometrics ASAP 2010 micropore-size analyzer. The specific surface area was determined using the linear portion of the BET model. Prior to these measurements, the samples were degassed in vacuum at 573 K for 2 h.

### 2.2.2. X-ray photoelectron spectroscopy

An AMICAS spectrometer (KROTAS instrument, Shimadzu) with an X-ray gun for Mg K $\alpha$  radiation was used. The XPS spectra were taken at room temperature in high vacuum to study the oxidation state of samples prior to reaction. The spectra were corrected with respect to the C 1s energy at 284.7 eV.

## 2.3. Kinetic investigation

The selective oxidation of DME was carried out in a fixed-bed quartz flow reactor. 50 mg catalyst sample was diluted with the same volume of acid-washed quartz powder (200 mg) in order to avoid temperature gradients in the catalyst bed. Prior to reaction, the catalyst was pre-oxidized in 10%  $O_2/He$  at 573 K for 1 h to clean out any possible impurities on the surface.

Two reactant gases were introduced through two parallel mass flow controllers. One gas mixture was 8.95% DME/4.5%  $N_2/He$  and  $N_2$  was used as an internal standard gas for product analysis. Another gas mixture was 10%  $O_2/He$ . The reactor effluents were analyzed by an online gas chromatograph equipped with TCD and FID detectors. A TDX-01 and Porapak Q combined packed column was used for the separation of  $O_2$ ,  $N_2$ , CO,  $CO_2$ ,  $H_2O$ , HCHO,  $CH_3OH$  and DME. A PLOT Q capillary column connected to the FID detector was used for the separation and detection of  $CH_4$ ,  $C_2H_4$ ,  $CH_3OH$ , DME, and methyl formate.

Reaction orders with respect to DME and oxygen were obtained by changing the flow rate of one gas mixture, while keeping the flow rate of another gas mixture constant. A balance gas of He was introduced to keep the total flow rate constant for all the runs reported here.

The effect of contact time on DME conversion and HCHO selectivity was studied at a constant ratio of

DME/ $O_2$ . The data was taken at 543 K for the  $VO_x/Al_2O_3$  catalyst, while it was taken at 553 K for the  $MoO_x/Al_2O_3$  catalyst due to its lower activity.

For the determination of the apparent activation energy and the pre-exponential factor, three runs were carried out by changing the molar ratio of DME to oxygen at different temperatures ranging from 513 to 573 K with a total flow rate of 40 ml/min.

## 3. Results and discussion

### 3.1. Structural and surface properties

The BET surface areas of supported 30 $MoO_3/Al_2O_3$  and 18 $V_2O_5/Al_2O_3$  were 162.1 and 184.2  $m^2/g$ , respectively. XRD measurements showed that the  $MoO_x$  is above the monolayer dispersion capacity of  $Al_2O_3$  and  $VO_x$  catalyst is slightly lower than the monolayer capacity.

XPS results for both catalysts prior to reaction are listed in figures 1 and 2. It can be seen that the Mo doublet exhibits binding energies at 235.8 eV for Mo 3d $_{3/2}$  and 232.7 eV for Mo 3d $_{5/2}$ , while V doublet exhibits binding energies at 517.6 eV for V 2p $_{3/2}$  and at 523.0 eV of V 2p $_{1/2}$ . Thus, the presence of  $Mo^{6+}$  species on the surface of  $Al_2O_3$  can be inferred [11,12]. By considering that standard binding energies of V 2p $_{3/2}$  for  $V^{5+}$ ,  $V^{4+}$  and  $V^{3+}$  are located at 517.2, 515.9 and 515.3 eV, respectively [13,14], the dominant presence of  $V^{5+}$  on the surface of  $Al_2O_3$  can be concluded.

### 3.2. Assessment of mass-transfer effect

For kinetic studies, the diffusions of the film (external) and the pores (internal) of the catalyst must be eliminated in order to obtain the intrinsic reaction rate. For the submillimeter particle size, the internal mass-transfer retardation usually does not affect gas-phase catalytic reactions. Here, it is considered that the selective oxida-

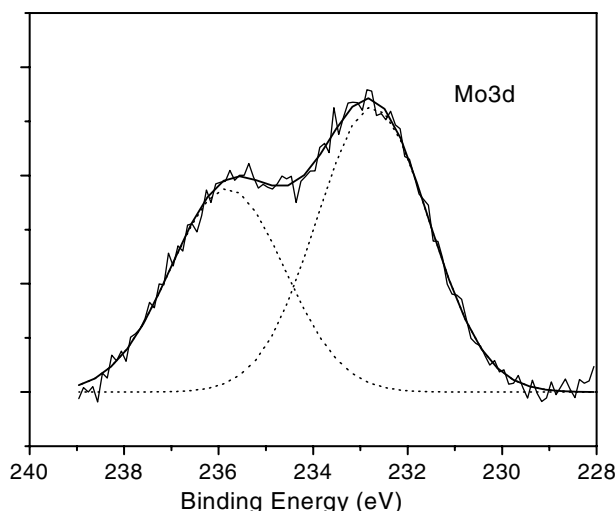
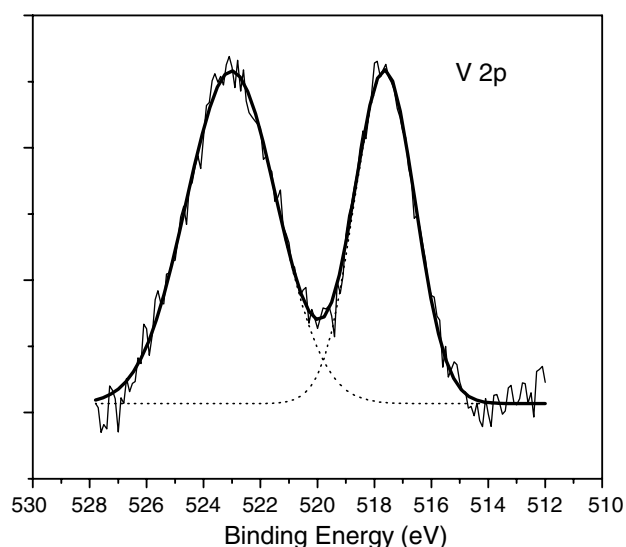


Figure 1. XPS spectra of the Mo 3d in  $MoO_x/Al_2O_3$  catalyst.

Figure 2. XPS spectra of the V 2p in  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst.

tion of DME is an internal diffusion-free reaction because the range of the catalyst particle size employed in the present study is between 250 and 450  $\mu\text{m}$ .

It is well known that oxidation reactions are fast, and thus, the flow rate should be large enough to avoid the existence of any external diffusion. In the present study, two preliminary runs with different amounts of  $\text{VO}_x/$

$\text{Al}_2\text{O}_3$  catalysts were performed at 553 K under a constant ratio of  $\text{DME}/\text{O}_2$  in the feed. The amount of catalyst in one of the runs was twice larger than that of the other. The feeding rates in these two cases were correspondingly adjusted to yield a constant  $F/W$ . It can be seen from table 1 that the conversion of DME was independent of the feeding rate. When the feeding rates were kept constant, the conversion with catalyst loading of 50 mg is about 2.5 times higher as that with 20 mg. These data were obtained in the  $F/W$  range of 27–200  $\text{ml/g}_{\text{cat}} \text{ min}$ , and the following kinetic investigations was carried out at a  $F/W$  range of 44–60  $\text{ml/g}_{\text{cat}} \text{ min}$ . Therefore the presence of any external mass-transfer resistance was precluded for the determination of reaction orders, the effects of contact time, and the apparent activation energies.

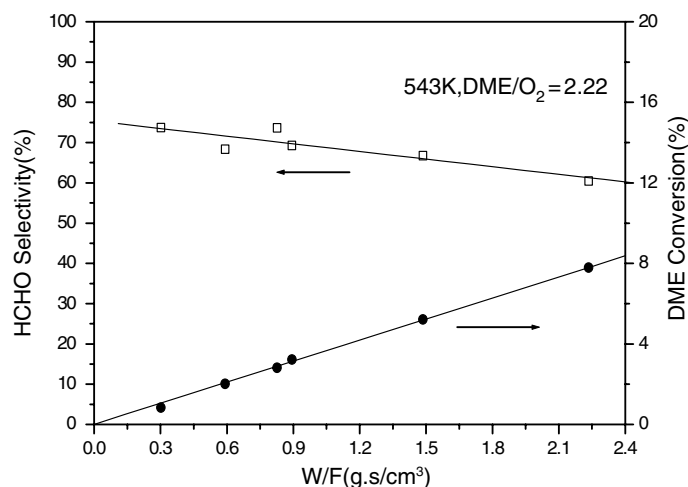
### 3.3. Effect of contact time

Figures 3 and 4 show the effect of contact time on the conversion of DME and the selectivity of formaldehyde on the  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst and the  $\text{MoO}_x/\text{Al}_2\text{O}_3$  catalyst.

It is clear that the conversion of DME increases linearly with contact time in both cases. The plots of contact time versus conversion of DME are straight lines passing through the origin of the coordinate, indicating that the selective oxidation of DME is a typical heterogenous catalytic surface reaction over the supported  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts.

Table 1  
Effect of external diffusion on the reaction over  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst

Temp. (K)	Cat $W$ (mg)	$F(\text{DME}/\text{He})$ (ml/min)	$F(\text{O}_2/\text{He})$ (ml/min)	$F(\text{He})$ ml/min	$F/W$ (ml/g <sub>cat</sub> min)	DME (conv. %)
553	25	5	6	14	17.9	13.6
50	10	12	28	17.9	12.6	
543	20	22.5	9	0	100.7	2.02
50	22.5	9	0	40.3	5.21	
20	15	6	0	67.1	3.2	
50	15	6	0	26.8	7.8	

Figure 3. Effect of contact time on the conversion of DME and the selectivity of formaldehyde on  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst.

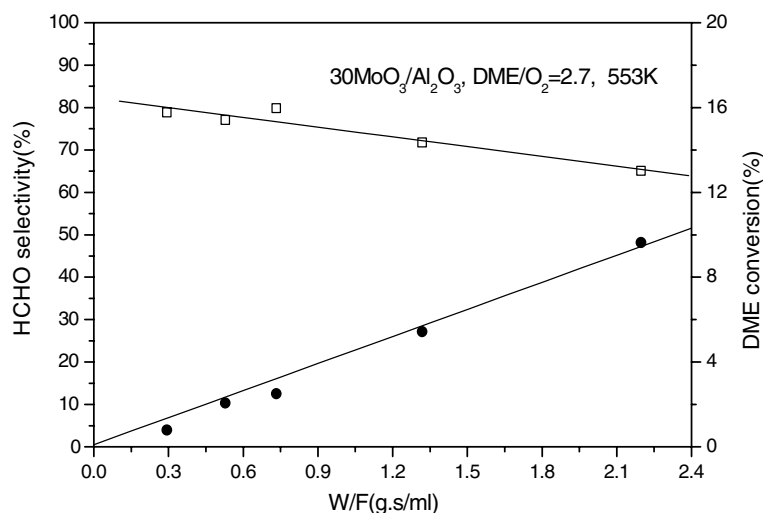


Figure 4. Effect of contact time on the conversion of DME and the selectivity of formaldehyde on  $\text{MoO}_x/\text{Al}_2\text{O}_3$  catalyst.

As can be seen from figures 5 and 6, the selectivity of HCHO decreases with the increasing in the contact time, while the selectivity to CO increases. This kind of formaldehyde selectivity dependence on the contact time suggests that the primary product in the partial oxidation of DME is HCHO. With the increase in the contact time, the initially formed HCHO would decompose into CO and  $\text{H}_2$ , or further oxidized to  $\text{CO}_2$  and  $\text{H}_2\text{O}$  on the catalyst surface. The primary selectivity of  $\text{CH}_3\text{OH}$  is not equal to zero, implying that it can be produced directly from DME.  $\text{CH}_3\text{OH}$  can be formed by intra-transfer of hydrogen between two  $\text{CH}_3\text{O}^*$  species. Moreover, the selectivity to  $\text{CH}_3\text{OH}$  is essentially independent of the contact time, suggesting that the further oxidation of methanol is a relatively slower process.

Meanwhile, the selectivity of CO, which is the main by-product of the reaction, increases with the contact time. This means that CO can be produced by secondary

reactions of HCHO. CO can also be formed directly by  $\text{CH}_3^*$  oxidation or by  $\text{CH}_3\text{O}^*$  decomposition. The selectivity of CO also increases with the reaction temperature, while the selectivity of  $\text{CO}_2$  and methyl formate are very small compared with that of CO.

$\text{CH}_4$  is observed over the  $\text{Al}_2\text{O}_3$  supported  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts only when the oxygen in the feed is depleted. This may suggest that the adsorbed  $\text{CH}_3^*$  species decomposed from DME is prone to combine with  $\text{O}^*$  to form  $\text{CH}_3\text{O}^*$  rather than to combine with the  $\text{H}^*$  that is dehydrogenated from the  $\text{CH}_3\text{O}^*$  species over these catalysts. But when the oxygen in the feed is completely depleted at about 593 K on  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst, DME would be decomposed into  $\text{CH}_4$  via the reaction of  $\text{CH}_3\text{OCH}_3 \rightarrow \text{CH}_4 + \text{CO} + \text{H}_2$  [8]. The decomposition of DME could be observed at 543 K when DME is the only feed-gas over supported  $\text{VO}_x$ . This means that the existence of oxygen inhibits the

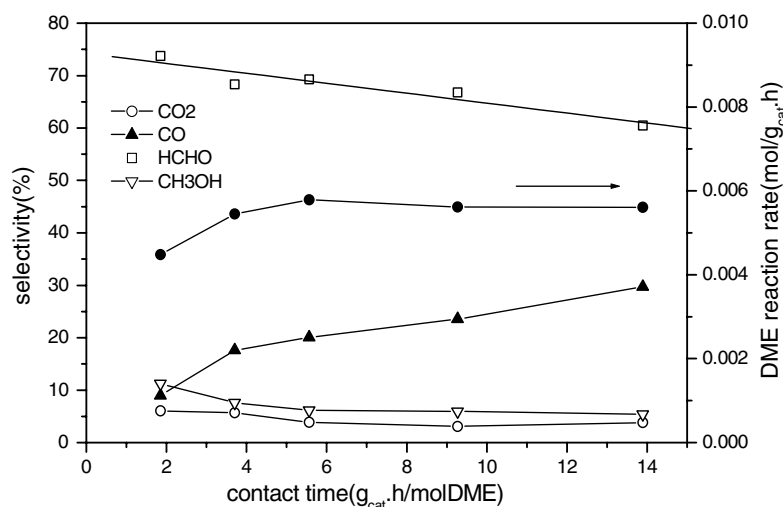
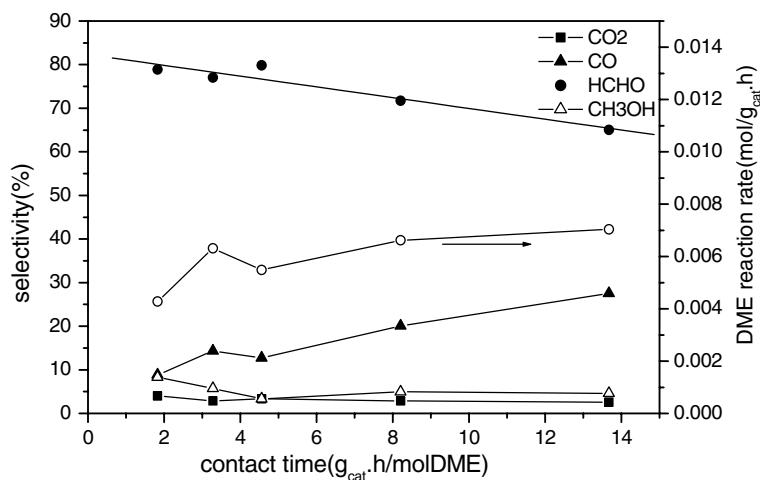


Figure 5. DME reaction rate and product selectivity over  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst at 543 K.

Figure 6. DME reaction rate and product selectivity over  $\text{MoO}_x/\text{Al}_2\text{O}_3$  catalyst at 553 K.

decomposition of DME, and favors the selective oxidation of DME to HCHO.

Thus, it can be seen that the oxidation of DME involves several products, such as HCHO, CO,  $\text{CO}_2$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{COOH}$  and  $\text{CH}_4$ . Formaldehyde is the main primary product while CO and  $\text{CH}_3\text{OH}$  are the dominant by-products. Methanol is formed by intra-transfer of hydrogen between two  $\text{CH}_3\text{O}^*$  species. CO can be produced directly by  $\text{CH}_3^*$  oxidation or  $\text{CH}_3\text{O}^*$  decomposition. CO can also be produced indirectly by secondary reactions of HCHO.

### 3.4 Apparent activation energies and pre-exponential factors

The activation energies and pre-exponential factors for the oxidation of DME were calculated according to

the Arrhenius plots over the  $\text{VO}_x$  and  $\text{MoO}_x$  catalysts. The results are summarized in tables 2 and 3, respectively.

The apparent activation energy for the conversion of DME is 122 kJ/mol and the pre-exponential factor is  $0.94 \times 10^6$  on the  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalysts. Although the activation energy for the formation of HCHO is slightly higher than that for the formation of  $\text{CH}_3\text{OH}$ , the pre-exponential factor for the formation of HCHO is nearly two orders of magnitude higher than that of  $\text{CH}_3\text{OH}$ . So the yield of HCHO is much higher than that of  $\text{CH}_3\text{OH}$ . In spite that the activation energy for CO formation is the highest, the highest pre-exponential factor for the formation of CO makes it the main by-product. The selectivity to  $\text{CO}_2$  is always low owing to the much smaller pre-exponential factor of  $\text{CO}_2$  formation.

Table 2  
Kinetic parameters over  $\text{VO}_x/\text{Al}_2\text{O}_3$  catalyst

	DME/ $\text{O}_2 = 1.48$		DME/ $\text{O}_2 = 2.66$		DME/ $\text{O}_2 = 5.03$		Average	
	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)
DME	118.9	$4.34 \times 10^5$	123.8	$1.37 \times 10^6$	122.7	$1.02 \times 10^6$	121.8	$0.94 \times 10^6$
HCHO	111.8	$5.99 \times 10^4$	116.4	$1.82 \times 10^5$	121.1	$4.47 \times 10^5$	116.4	$2.30 \times 10^5$
CO	150.2	$1.00 \times 10^8$	155.4	$3.19 \times 10^8$	145.2	$3.33 \times 10^7$	150.3	$1.51 \times 10^8$
$\text{CO}_2$	82.8	5.31	80.9	3.63			81.9	4.47
$\text{CH}_3\text{OH}$	106.1	$1.19 \times 10^3$	114.7	$1.35 \times 10^3$	111.7	$8.27 \times 10^3$	110.8	$3.60 \times 10^3$

Table 3  
Kinetic parameters over  $\text{MoO}_x/\text{Al}_2\text{O}_3$  catalyst

	DME/ $\text{O}_2 = 1.54$		DME/ $\text{O}_2 = 2.76$		DME/ $\text{O}_2 = 4.83$		Average	
	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)	$E_a$ (kJ/mol)	$A$ (mol/gcat · s)
DME	128.5	$2.17 \times 10^6$	119.5	$3.12 \times 10^5$	128.3	$1.89 \times 10^6$	125.4	$1.46 \times 10^6$
HCHO	121.6	$3.66 \times 10^5$	117.3	$1.44 \times 10^5$	125.2	$7.37 \times 10^5$	121.4	$4.16 \times 10^5$
CO	165.0	$1.02 \times 10^9$	141.8	$6.72 \times 10^6$	158.0	$1.61 \times 10^8$	154.9	$3.94 \times 10^8$
$\text{CH}_3\text{OH}$	102.8	$4.03 \times 10^2$	100.4	$2.90 \times 10^2$	118.1	$7.33 \times 10^3$	107.1	$2.67 \times 10^3$

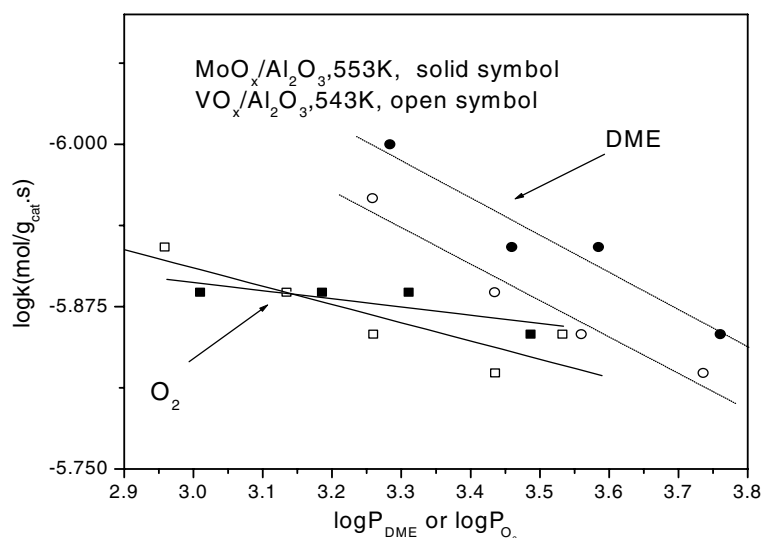


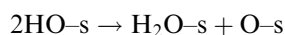
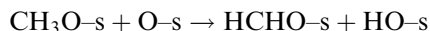
Figure 7. Reaction orders with respect to DME and  $O_2$ .

The activation energies and pre-exponential factors for DME conversion and product formation on the  $MoO_x/Al_2O_3$  catalyst were also calculated. The observed kinetic behaviors on the  $MoO_x/Al_2O_3$  catalyst are very similar to that on the  $VO_x/Al_2O_3$  catalyst.

### 3.5. Reaction orders

The reaction result for the determination of the reaction orders with respect to DME and  $O_2$  is listed in figure 7. The reaction rates did not change markedly with the variation in either the oxygen concentration or the DME concentration. Therefore, the reaction was pseudo-zero order with respect to the DME and the  $O_2$  partial pressures employed. Increase of the gas phase concentration has little effect on the reaction rate.

This also means that DME can be initially decomposed easily into adsorbed  $CH_3$  and  $CH_3O$  species on the  $MoO_x$  and  $VO_x$  catalyst surfaces [15]. Selective oxidation of DME is controlled by reactions of the saturated intermediates adsorbed. The zero-order dependence of  $O_2$  indicates that the transformation of oxygen molecule into lattice oxygen, and the rapture of O species by dissociated  $CH_3^*$  to form  $CH_3O^*$  could not be the rate-limiting step. The reaction rate is most likely to be limited by the C–H bond activation of the adsorbed  $CH_3O^*$  intermediate via a redox mechanism by using the lattice oxygen atoms as depicted following.



## 4. Conclusions

Kinetics of DME oxidation has been investigated over  $Al_2O_3$ -supported  $VO_x$  and  $MoO_x$  catalyst near

their monolayer capacity loadings. The effects of contact time on DME conversion and HCHO selectivity indicates that the reaction only takes place on the surface of the catalyst, and HCHO is the main primary product. The apparent activation energies for the conversion of DME were found to be 122 kJ/mol over the  $VO_x/Al_2O_3$ , and 125 kJ/mol over the  $MoO_x/Al_2O_3$ , respectively. The reaction is pseudo-zero order with respect to both DME and  $O_2$  under the reaction conditions employed, suggesting that the most likely rate-determining step is the oxy-dehydrogenation of the  $CH_3O^*$  species.

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