

Spherical Wave Near-Field Imaging and Radar Cross-Section Measurement

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Abstract—The paper presents a new inverse synthetic aperture radar (ISAR) algorithm intended for radar cross-section (RCS) imaging and measurement from scattered fields. The method, based on a spherical-wave near-field illumination of the target, overcomes the requirement for an expensive compact range facility to produce a plane wave illumination. The formulation and the implementation of the algorithm are described. Some experimental results obtained in an anechoic chamber are presented to show RCS results similar to the conventional plane wave methods.

I. INTRODUCTION

A radar target is characterized by its radar cross section (RCS), which, for a given object and polarization set, depends on both the frequency and the observation angle. For analysis and diagnostics, inverse synthetic aperture radar (ISAR) techniques [1] are usually applied to the RCS data to obtain high-resolution images of the target radar reflectivity spatial distribution. The RCS is obtained by illuminating the radar target with a uniform plane wavefront and measuring the scattered fields [2]; for high frequencies or large targets, however, the plane wave illumination becomes difficult to produce with the required accuracy.

The RCS can be measured in a far-field range requiring a long distance between target and antennas. Alternatively, a compact range in an anechoic chamber requires a high-quality reflector and suffers from edge diffraction which limits the size of the quiet zone (volume where the illumination can be considered a plane wave).

To overcome these problems, an alternative procedure based on near-field measurements using spherical wavefronts from low-directivity antennas has been developed.

This new algorithm consists of two parts: 1) *high-resolution spherical wave imaging*, which obtains the radar reflectivity image of the target from the scattered measurements using a spherical wave near-field illumination [3] and 2) *RCS calculation and calibration* using the known relationship between reflectivity and RCS in conventional ISAR techniques [4].

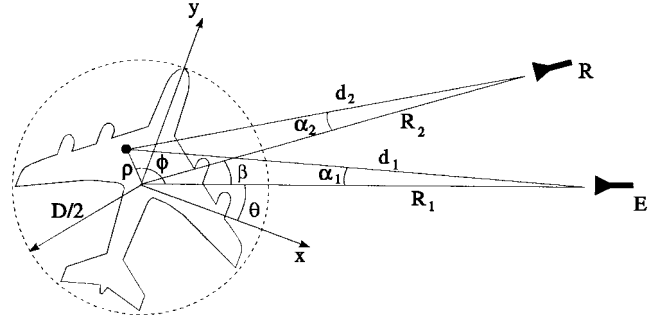


Fig. 1. Geometrical parameters of the stated problem.

II. PROBLEM STATEMENT

Consider the setup illustrated in Fig. 1 in which an object of maximum dimension D (which is assumed to be planar and contained in the $z = 0$ plane) with coordinates (x, y) and formed by a distribution of independent and nondirectional scatterers of reflectivity $\psi(\rho, \phi)$ is rotated by a scan angle θ with respect the origin.

An emitter antenna (E), located at a distance R_1 from the rotation center and with a radiation pattern $G_E(\alpha)$, radiates an electromagnetic field that illuminates the object.

The scattered fields E_S are measured by a receiver antenna (R) with a radiation pattern $G_R(\alpha)$ and located at a distance R_2 from the center, but separated by bistatic angle β from the emitter.

Integrating the contribution of each scatterer we obtain

$$E_S(f, \theta) = \int_0^\infty \int_0^{2\pi} C \cdot \psi(\rho, \phi) \frac{e^{-j \frac{2\pi}{\lambda} (d_1 + d_2)}}{d_1 \cdot d_2} \times G_E(\alpha_1) \cdot G_R(\alpha_2) \cdot \rho d\rho d\phi \quad (1)$$

where C is a constant depending on the parameters of the system that can be removed with calibration and where the distances from the emitter and receiver antennas to each scatterer (d_1, d_2) and the illumination angles (α_1, α_2) can be easily obtained from the geometry

$$\begin{aligned} d_1 &= \sqrt{R_1^2 + \rho^2 - 2 \cdot R_1 \cdot \rho \cdot \cos(\phi - \theta)} \\ d_2 &= \sqrt{R_2^2 + \rho^2 - 2 \cdot R_2 \cdot \rho \cdot \cos(\phi - \theta - \beta)} \\ \alpha_1 &= \arcsin\left(\frac{\rho \cdot \sin(\phi - \theta)}{d_1}\right) \\ \alpha_2 &= \arcsin\left(\frac{\rho \cdot \sin(\phi - \theta - \beta)}{d_2}\right). \end{aligned}$$

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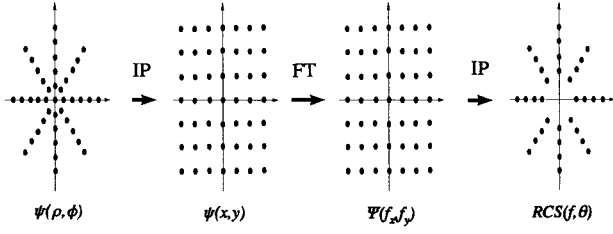


Fig. 2. Procedure to obtain RCS from reflectivity image.

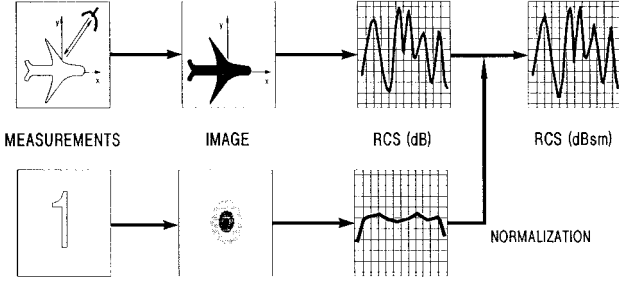


Fig. 3. RCS obtention from near-field scattering measurements.

Note that if $R_1, R_2 \gg \rho$ and $\beta = 0$, the plane wave monostatic case is recovered as should be expected since

$$\begin{aligned} R_1 &= R_2 = R \\ \alpha_1 &= \alpha_2 = \alpha \\ d_1 &= d_2 \\ d_1 + d_2 &\rightarrow 2 \cdot (R - \rho \cdot \cos(\phi - \theta)) \\ d_1 \cdot d_2 &\rightarrow R^2. \end{aligned}$$

Under these conditions, $E_S(f, \theta)$ can be expressed as a bi-dimensional Fourier transform of the reflectivity distribution.

III. SPHERICAL WAVE IMAGING

Imaging the target's radar reflectivity is a useful tool for identifying scattering mechanisms. The scattered fields E_S can be measured over a range of frequency and azimuth and the reflectivity image ψ can then be obtained by coherently focusing the field given in (1) on the image domain.

In mathematical terms

$$\psi(\rho, \phi) = \int_0^\infty \int_0^{2\pi} E_s(f, \theta) \cdot \xi(f, \theta, \rho, \phi) df d\theta.$$

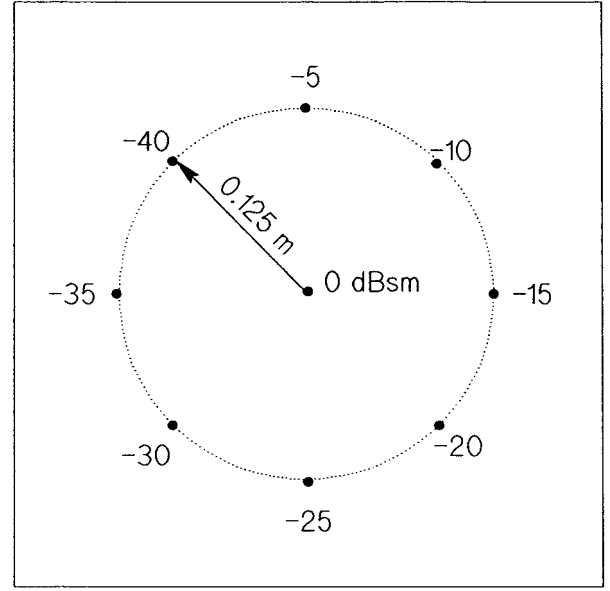
The reflectivity image is obtained by applying a focusing operator $\xi(f, \theta, \rho, \phi)$ to each scattered field measurement for a given frequency and scan angle (f, θ) , which restores changes incurred by the amplitude and argument of the wave on its way to and from the scatterer located at the position (ρ, ϕ) .

Accordingly, the expression for the focusing operator is

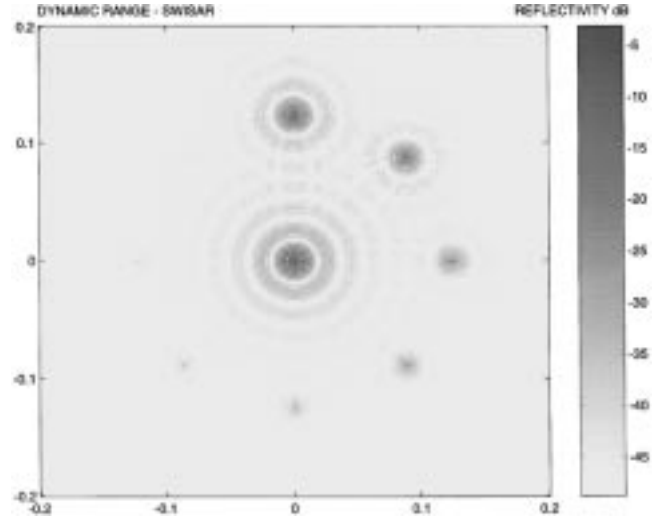
$$\xi(f, \theta, \rho, \phi) = \frac{e^{j \frac{2\pi}{\lambda} (d_1 + d_2)} \cdot d_1 d_2}{G_E(\alpha_1) \cdot G_R(\alpha_2)} \cdot f$$

Then we have

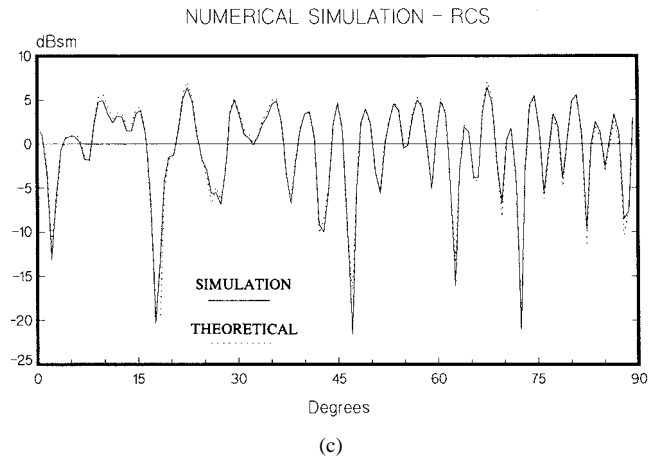
$$\psi(\rho, \phi) = \int_0^\infty \int_0^{2\pi} E_s(f, \theta) \cdot \frac{e^{j \frac{2\pi}{\lambda} (d_1 + d_2)} \cdot d_1 d_2}{G_E(\alpha_1) \cdot G_R(\alpha_2)} \cdot f df d\theta. \quad (2)$$



(a)



(b)



(c)

Fig. 4. (a) Target modeled to evaluate the dynamic range. (b) Reflectivity image of the modeled target. (c) RCS curves of the modeled target.

This expression is the transform pair of (1); moreover, when $R \gg \rho$ and $\alpha = 0$, the previous expression becomes a bi-

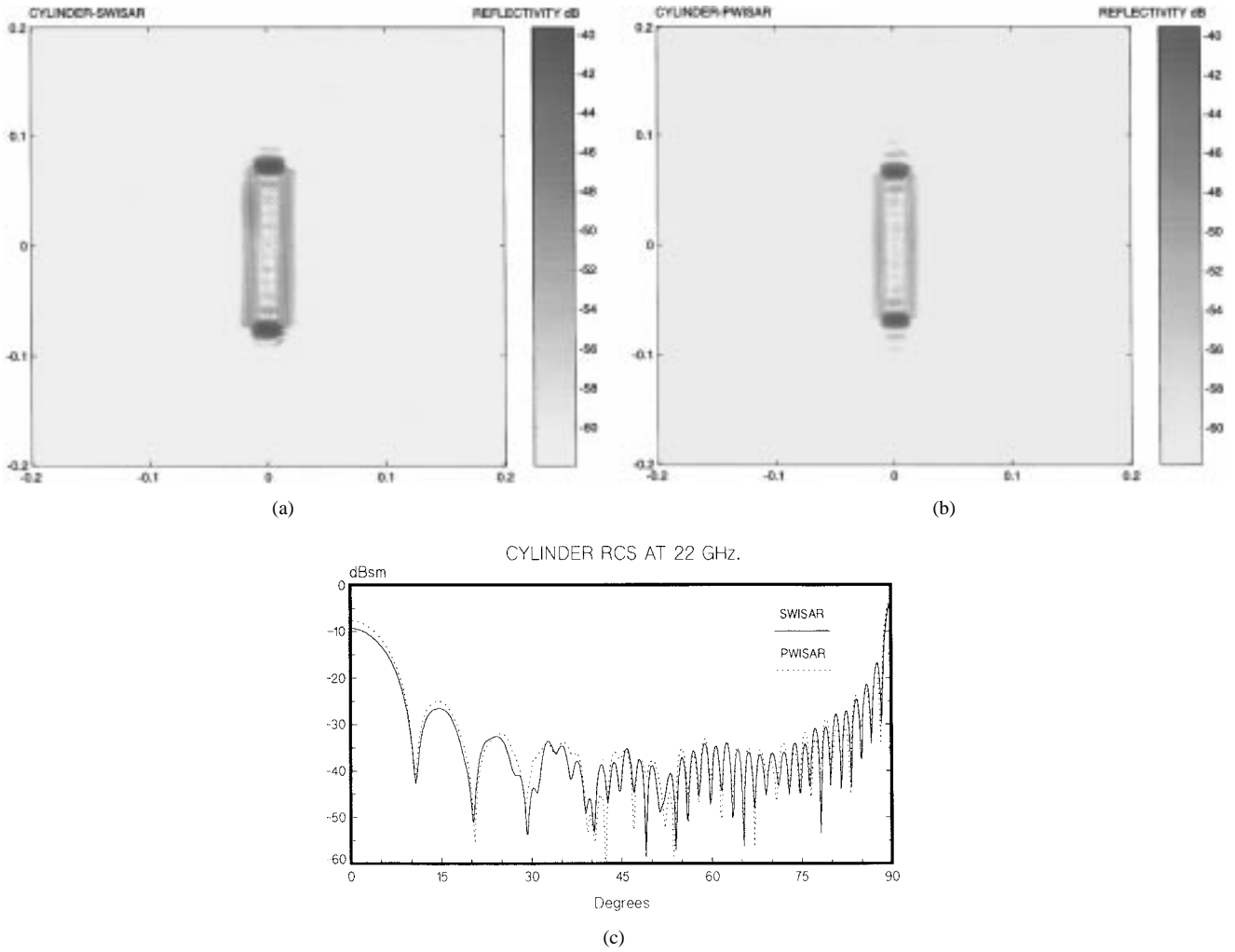


Fig. 5. (a) Cylinder image obtained with the SWISAR algorithm. (b) Cylinder image obtained with the conventional methods. (c) RCS curves of the cylinder.

dimensional inverse Fourier transform in polar coordinates, which is precisely the conventional ISAR technique to obtain the reflectivity image from the scattering fields produced with a plane wavefront [1].

IV. RCS CALCULATION

It is well known [1] that if a target formed by independent and nondirectional scatterers is illuminated with a plane wavefront in a monostatic geometry, the coherent superposition of fields scattered from each element corresponds to the total scattered field of the target at each frequency and scan angle

$$\sigma(f, \theta) = e^{-j2\frac{2\pi}{\lambda}R} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \psi(x, y) e^{j2\frac{2\pi}{\lambda}(x \cos \theta + y \sin \theta)} dx dy.$$

Since this value is closely related to the RCS one, from now on it will be called indistinctly RCS. In fact, we have

$$\text{RCS}(f, \theta) = |\sigma(f, \theta)|^2.$$

Apart from constants, this expression is identical to a bi-dimensional Fourier transform of the reflectivity image

expressed in Cartesian coordinates. The RCS can, therefore, be determined as a sample of the bi-dimensional Fourier spectrum of the reflectivity image

$$\begin{aligned} \Psi(f_x, f_y) &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \psi(x, y) \cdot e^{-j2\pi(x \cdot f_x + y \cdot f_y)} dx dy \\ \Rightarrow \sigma(f, \theta) &= \Psi(f_x, f_y)|_{f_x = -\frac{2}{\lambda} \cos \theta, f_y = -\frac{2}{\lambda} \sin \theta}. \end{aligned}$$

The numerical values of the RCS parameter finally obtained are affected by a constant that depends on the frequency and azimuth ranges of the measurement and other parameters. Thus, a calibration of the results will be needed in order to obtain absolute RCS values.

V. ALGORITHM IMPLEMENTATION

Equation (2) is computed using a circular convolution algorithm over the azimuth angle: since ξ is a function of $(\phi - \theta)$ and E_s is a function of only (θ) , the integration in θ can be interpreted as a circular convolution which can be easily computed as a product in the Fourier spectral domain.

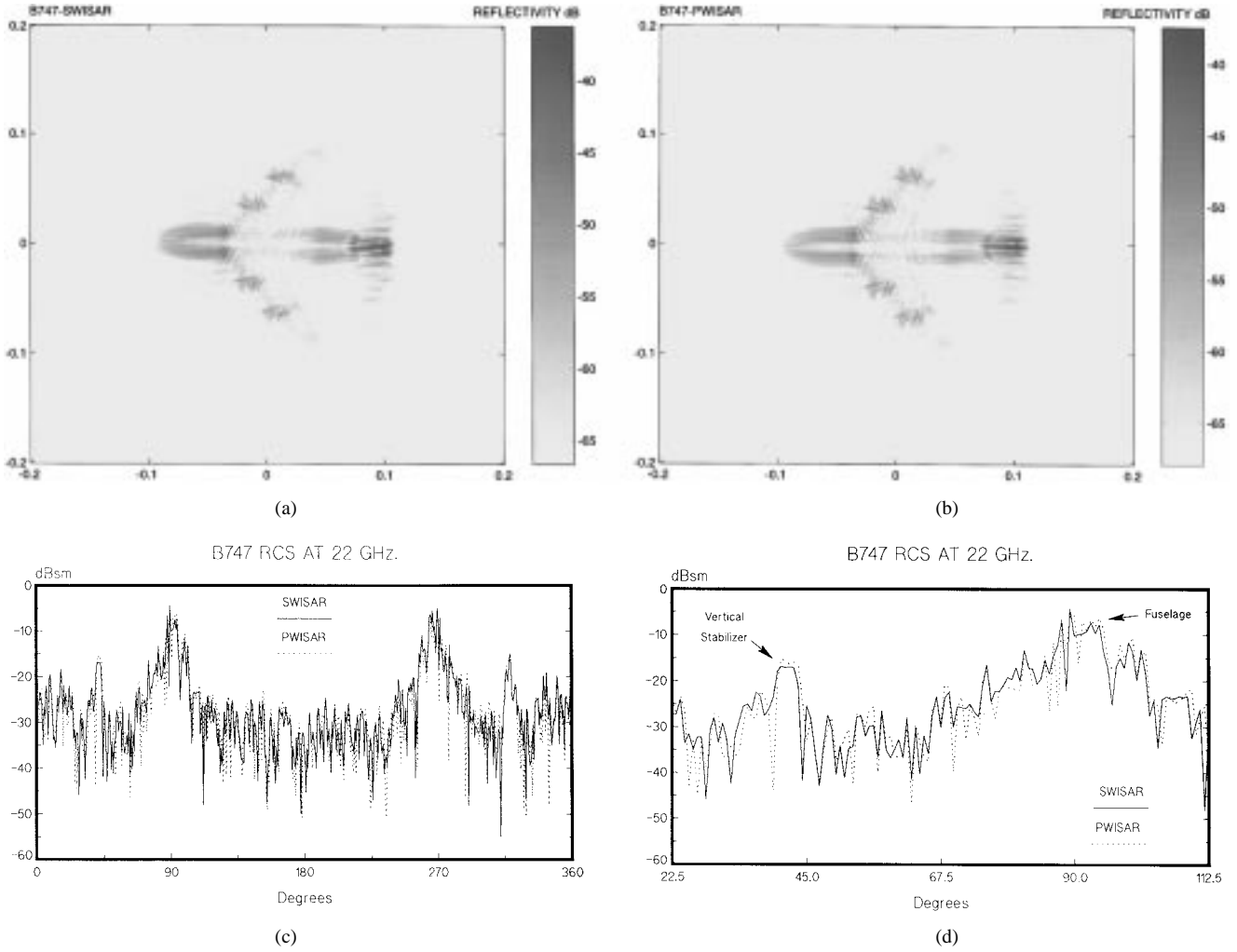


Fig. 6. (a) B747 image obtained with the SWISAR algorithm. (b) B747 image obtained with the conventional methods. (c) RCS curves of the B747. (d) RCS curves of the B747 (detail).

A similar approach has been applied for plane waves [5]:

$$\begin{aligned}
 \psi(\rho, \phi) &= \int_0^\infty \int_0^{2\pi} E_s(f, \theta) \cdot \xi(f, \rho, \phi - \theta) df d\theta \\
 &= \int_0^\infty E_s(f, \theta) * \xi(f, \rho, \phi) df \\
 \psi(\rho, \phi) &= \sum_f E_s(f, \theta) * \xi(f, \rho, \phi) \\
 &= \sum_f \text{IFFT}_\phi[\text{FFT}_\phi[E_s(f, \theta)] \cdot \text{FFT}_\phi[\xi(f, \rho, \phi)]]
 \end{aligned}$$

The required normalization factors can be computed using the advantage that $\xi(f, \rho, \phi)$ for a given system is constant; therefore, storing its fast Fourier transform (FFT) values on disk reduces the computation time.

Having obtained the reflectivity image, the following three steps shown in Fig. 2 are required to obtain the RCS values:

- Bi-dimensional interpolation: $\psi(x, y) = \psi(\rho, \phi)$
 $|x = \rho \cos \theta, y = \rho \sin \theta$;
- Bi-dimensional Fourier transform: $\Psi(f_x, f_y) = \text{FFT}_{2D}[\psi(x, y)]$;
- Bi-dimensional interpolation: $\sigma(f, \theta) = \Psi(f_x, f_y)$
 $|f_x = -\frac{2}{\lambda} \cos \theta, f_y = -\frac{2}{\lambda} \sin \theta$.

Having obtained the RCS parameter, we address the calibration problem. The reference used to obtain absolute values is the point spread function (PSF), which is simply a point scatterer of unitary RCS located at the origin of coordinates, which can also be interpreted as the bi-dimensional impulse response of the imaging procedure.

The calibration uses the observation that the scattered fields and the recovered RCS of the PSF have to be one. The calibration consists of dividing, for each frequency and scan angle, the calculated target RCS by the one obtained being the PSF the input of the process. If the object were the PSF, therefore, resulting value would be correctly one. Fig. 3 shows the global procedure followed.

VI. ADDITIONAL ADVANTAGES

This new algorithm, called spherical wave ISAR SWISAR, has additional advantages apart from simplicity and accuracy: owing to the focusing operator ξ , effects as the nonisotropic radiation patterns of the antennas and the existence of a bistatic angle can be completely incorporated to the algorithm with no additional complication as indicated by (2). Using nonisotropic antennas it is possible to focus the power on the target and, in addition, reduce the undesired reflections on the anechoic

chamber and the coupling between the emitter and receiver antennas.

On the other hand, when monostatic measurements are required, two close in-space antennas are often used in a slightly bistatic geometry; this gives approximated results according to the bistatic equivalence theorem. The SWISAR approach avoids this approximation because the formulation accounts for bistatic geometries.

VII. RESULTS

The procedure has been tested with numerical simulations and experimental results and it shows that the reflectivity images and the RCS curves are quite similar to those obtained with a plane wavefront, both in shape and in absolute values.

Numerical simulations have been used for a preliminary validation of the new method. Fig. 4 shows the results corresponding to a radar target modeled by a number of point scatterers on a wide amplitude range [Fig. 4(a)]: the reconstructed reflectivity image [Fig. 4(b)] shows that the dynamic range of the SWISAR algorithm is around 40 dB, while the good correlation between the theoretical and calculated RCS curves [Fig. 4(c)] leads to the validation of the new algorithm for targets formed by independent point-like scatterers. Some targets cannot be adequately modeled by a group of independent scatterers. Although this assumption is always adopted in ISAR formulation (either with plane or with spherical wave illumination methods), multiple scattering mechanisms like double reflections do appear in the radar reflectivity image [1]. Since the RCS values are obtained from that image, multiple scattering contributions will be also present in the resulting RCS.

This point has been assessed experimentally in an anechoic chamber using metallic cylinders and plane models as targets. Both spherical and plane waves have been used for the illumination. The instrumentation is based on the HP8510 network analyzer, which allows a basic calibration with a reference target and time gating of the quiet zone in order to avoid undesired reflections. The measurements have been made in the K-band (18–26 GHz) over the entire angular range (360°) with the antennas using in the horizontal–horizontal (HH) polarization. The radiation patterns of the antennas have been characterized and incorporated to the algorithm. The distances from the antennas to the origin have been $R_1 = R_2 = 1.3$ m and the bistatic angle between them $\beta = 3.3^\circ$.

From numerical simulations it has been found that the minimum distance between target and antennas is two-dimensional (2-D), D being the maximum azimuth dimension of the target; shorter distances will lead to high-power differences between the center of the target and its periphery that could surpass the dynamic range of the system and amplify the noise effects.

Fig. 5 shows the results obtained from a cylinder 228 mm high and 45 mm wide. Because the cylinder is a canonical target widely studied, the reflectivity image and RCS response are well known. The images reconstructed with the SWISAR algorithm and the conventional methods are presented in Fig. 5(a) and (b) and the superposition of the RCS curves at 22 GHz obtained with both procedures are shown in Fig. 5(c).

Fig. 6 shows the results for a complex radar target consisting of a metallized Boeing 747 model (1:200 scale). Similarly,

the reflectivity images reconstructed from spherical and plane wavefront illuminations are shown in Fig. 6(a) and (b) and the superimposed RCS curves at 22 GHz are shown in Fig. 6(c). The region of these curves corresponding to the higher reflectivity areas (fuselage and vertical stabilizer) are marked to indicate the high correlation between the two curves [Fig. 6(d)].

VIII. CONCLUSION

While microwave imaging, object recognition, and radar target modeling are gaining increasing interest and application, a serious practical problem appears in the creation of the desired plane wavefront needed to carry out the RCS measurements. The problem is especially acute in high-frequency reconstructions of large objects.

An alternative RCS measurement procedure based on spherical wavefront near-field scattering measurements has been presented, which is much easier to obtain.

The measurement distance can be reduced to twice the maximum azimuth dimension of the target and although far-field conditions must be still satisfied in the vertical dimension, most of the radar targets fit the required geometry quite well.

Apart from that, the illumination frequency can be increased without any technical problem while producing the spherical wavefront. Deviations from an ideal spherical wave can be taken in account in the algorithm by characterizing the radiation patterns of the antennas.

This technique is being extended now to three-dimensional scatterers for cylindrical and spherical scanning geometries [6].

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