

# A Retrodirective Microstrip Antenna Array

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**Abstract**—A Van Atta retrodirective reflector was designed and developed, using an aperture-coupled microstrip antenna array. This reflector possesses the advantage of reflecting high fields to the source point over a wide range of incidence angles and, owing to the low cost and conformability of the structure, is suitable for applications in intelligent vehicle highway systems (IVHS). An approximate theory associated with the reradiation and scattering principles of the reflector is presented for the purpose of understanding and designing the reflector. The utility of the retrodirective reflector was demonstrated by comparison with a plate reflector and a microstrip antenna array without a feed structure. Finally, a reflector with switches in the middle of the microstrip feed lines was investigated for possible applications in communications and remote identification.

**Index Terms**—Microstrip antenna arrays, microstrip patch antenna, retrodirective antenna.

## I. INTRODUCTION

**D**UE to the swift decline of military spending and rapid advancement of component technology, microwave, and millimeter-wave systems have moved from military applications to commercial ones over the past few years [1]–[6]. Two interesting applications in the commercial area are automotive collision avoidance and road traffic management, both playing important roles in future intelligent vehicle highway systems (IVHS). The former provides the services of warning the driver of potential hazards in his path, including vehicles and roadside obstacles. The latter contains several aspects of road transport informatics and may be accomplished by the communications between vehicles and roadside beacons [1].

For automotive collision avoidance, many researchers have focused on the developments of vehicle radars, including forward-looking, backward-looking, and sideward-looking radars [2], [3]. These radars emit modulated continuous waves (CW) or pulsed waves and receive echoes from other vehicles or roadside obstacles (man-made traffic structures, topographic structures, etc.). Information such as distance and speed, can then be read from the echoes to produce warning signals. However, the echo from a vehicle relies on scattering from the vehicle body and is narrow beamed. Only near normal directions to the body surface can a high reflected field be obtained. The higher the frequency used, the narrower the reflected beam is (for a given antenna size). Therefore, outside the return signal beamwidth the radar can not receive any response. One possible solution to this limitation of the

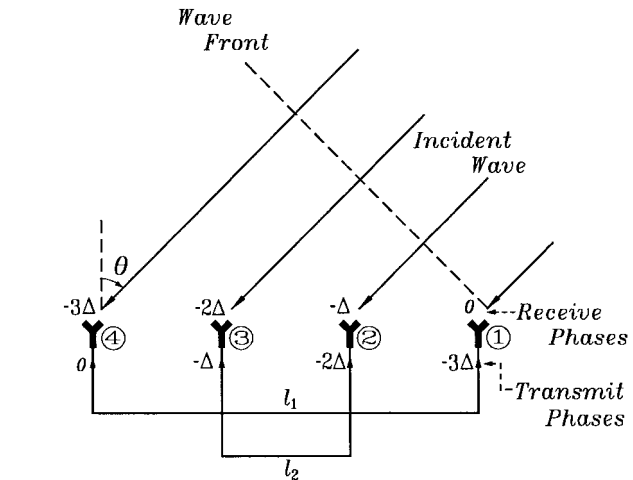


Fig. 1. A four-element Van Atta retrodirective array.

radar is to increase the scattering beamwidth of vehicles, which can be achieved by placing retrodirective reflectors on the vehicle surfaces and road obstacles.

In this paper, we describe a Van Atta retrodirective reflector using a microstrip antenna array. The concept of this reflector was first proposed by L. C. Van Atta [7] and it possesses the advantage that the field reradiated by the reflector has a maximum in the direction of the incident plane wave. Fig. 1 illustrates a reflector composed of four antennas. Antennas 1 and 4 are paired by a transmission line of length  $l_1$ , and antennas 2 and 3 are by a line of length  $l_2$ . A plane wave is incident upon the array at an angle  $\theta$ , which introduces a receiving phase lag of  $\Delta (= k_o d \sin \theta)$  between the adjacent antennas. ( $k_o = 2\pi/\lambda_o$  is the free-space propagation constant and  $d$  is the distance between antennas.) The signals received by antenna 1 and antenna 2 are fed through the transmission lines to antenna 4 and antenna 3, respectively, and vice versa. If the difference between  $l_1$  and  $l_2$  equals a multiple of the wavelength in the transmission lines, a feeding phase excess of  $\Delta$  exists between the antennas, thus forcing the antenna array to radiate toward the direction from which the incident wave comes.

After the report of L. C. Van Atta, many investigations of this type of reflector were done using dipole antennas or horn antennas [8]–[11]. Instead of a pure passive configuration, some also added bidirectional amplifiers or mixers in the transmission lines to enhance and/or modulate the echoes [12]. The applications of the Van Atta reflector have been proposed in satellite communication [13] and in enhancing the radar cross sections of ships and airplanes [14].

The proposed microstrip antenna type of Van Atta reflector has the advantages of easy design, low cost, and great

Manuscript received August 5, 1996; revised July 8, 1998.

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Publisher Item Identifier S 0018-926X(98)09685-9.

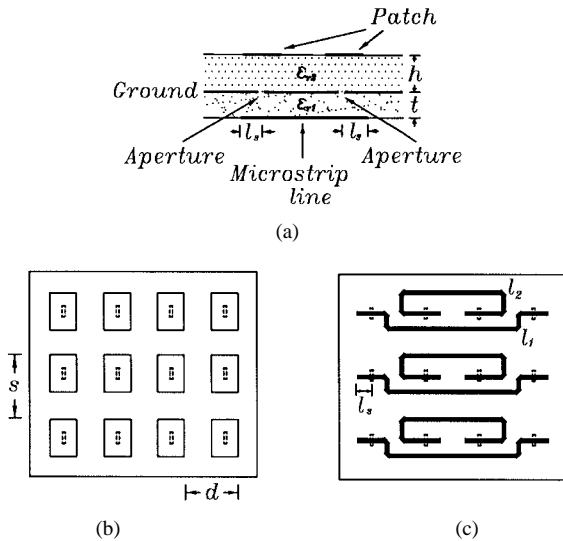


Fig. 2. (a) The (partial) side view. (b) The top view. (c) The bottom view of a retrodirective aperture-coupled microstrip antenna array. The apertures (dashed lines) are located on the ground plane between (b) the antenna substrate and (c) the circuit substrate.

conformability to a given surface shape and is thus a good candidate for use in the abovementioned vehicle collision avoidance radar and obstacle warning systems. Another application of this array reflector is in road traffic management, where it can be furnished in a vehicle as an on-board unit [4] to communicate with roadside beacons. To do this, switches or amplifiers might be incorporated in the array reflector. By controlling the on-off states of such switches or amplifiers, the array can reflect the amplitude modulated signals to the beacons. Owing to the retrodirective effect of this on-board unit, the vehicle can have a large communication angle and range with beacons [4]. These semi-active (switches) or active (amplifiers) retrodirective reflectors can also be used in remote identification of persons or vehicles [6]. By adding identification binary codes to control the switches or amplifiers, the reflectors can return coded responses to the interrogators.

## II. DESIGN OF MICROSTRIP ANTENNA

Fig. 2 shows the new retrodirective reflector. A two-layer configuration was used in this design [Fig. 2(a)]. Three identical E-plane subarrays were made to enhance the echo of the reflector. Each linear subarray contains two pairs (four elements) of aperture-coupled microstrip antennas [Fig. 2(b)] fed by two equal-length microstrip lines ( $l_1 = l_2 = l$ ) on the reverse side of the ground plane [Fig. 2(c)]. To reduce the influence of the mutual couplings between antennas, the distances between subarrays ( $s$ ) and between subarray elements ( $d$ ) are set equal to 21 and 18 mm, respectively, which are  $0.7\lambda_0$  and  $0.6\lambda_0$  for a frequency of 10 GHz. The thickness ( $t$ ) and the relative dielectric constant ( $\epsilon_{r1}$ ) of the circuit substrate are 0.508 mm and 2.2, respectively, resulting in a width of 1.6 mm for a 50- $\Omega$  microstrip feed line. The antenna substrate has a thickness ( $h$ ) of 0.787 mm and a relative dielectric constant ( $\epsilon_{r2}$ ) of 2.3. To reduce the interference caused by the scattering

from the ground plane, the whole size of the reflector is kept as small as possible and is measured to be  $76 \times 68 \text{ mm}^2$ .

The antenna and the feed structure were designed using a commercial program, PCAAD [15]. The widths of the microstrip antenna and the microstrip feed line were 12 mm and 1.6 mm, respectively. The other parameters were then varied to produce a 50- $\Omega$  input impedance (seen by the feed line) at a frequency of 10 GHz, so that maximum power can be received by the microstrip line from one antenna and be reradiated from the other antenna of the same pair. The computed length of the antenna, size of the aperture, and length ( $l_s$ ) of the microstrip matching stub line are 8.73 mm,  $4 \times 1 \text{ mm}^2$ , and 5 mm, respectively. To verify the aperture-coupled antenna design, a separate single-element aperture-coupled microstrip antenna was made and measured. A return loss of as low as -19 dB at the center frequency of 10.025 GHz was obtained, which ensured the validity of the design.

Although putting the feed lines on the same plane as the antennas can reduce complexity, the aperture-coupled configuration was chosen due to two considerations. First, the microstrip lines in the coplanar design may produce extra radiation, deteriorating the performance of the reflector. Although not shown in this paper, this has been verified for the configuration with antennas directly fed by high-impedance lines (170  $\Omega$ ) and for that with antennas fed by medium impedance lines (85  $\Omega$ ) through quarter-wavelength transformers (120  $\Omega$ ). (Microstrip lines of 50  $\Omega$  are too wide to be incorporated on the antenna plane.) Second, since no antenna appears in the circuit substrate for the aperture-coupled structure, there is more space and, thus, more flexibility for routing of the microstrip lines. Also, it is easier to add other solid-state circuits such as switches or amplifiers (if needed) in the aperture-coupled structure.

## III. THEORY OF RETRODIRECTIVE MICROSTRIP-ANTENNA REFLECTOR

For a better understanding of the proposed retrodirective reflector, an approximate theory was developed to analyze the structure. The field returning to the source point of the plane wave is primarily composed of three parts: the reradiated field, the scattered field from the terminated patch antennas [16], and the scattered field from the partially covered ground plane. When a wave is incident upon an array, some of the power is captured by the antennas and then reradiated from corresponding antennas of the same pairs [Fig. 3(a)], causing a reradiated field to the source point. In addition, some of the power is scattered by the microstrip patches and by the partially covered ground plane, which contributes to the two scattered field components. The scattered field from the patch antennas comes from the patch currents induced by the incident wave. For simplicity, these currents are approximated as physical optics (PO) currents [17]. The radiation of the edge currents induced on the patches is ignored. Thus, since the antenna substrate is thin enough (as compared to the wavelength) to be ignored, a flat metal plate of the same size ( $L \times W = 76 \times 68 \text{ mm}^2$ ) as the ground plane is used to compute the total scattered field [Fig. 3(b)]. In the following analysis,

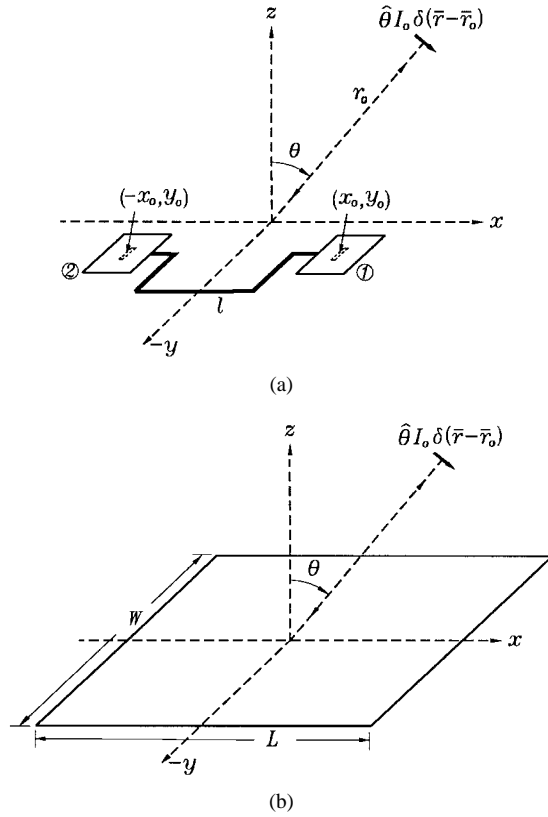


Fig. 3. (a) A pair of aperture-coupled microstrip antennas for analyzing the reradiated fields. (b) A flat metal plate used to calculate the scattered fields.

the feed lines and the antennas are assumed to be matched so that no reflection field is excited when a guided field is fed from a feed line to an antenna. The mutual couplings between antennas and possibly between microstrip lines are neglected. Also, the diffraction of the reradiated field by the ground plane edges is ignored.

Fig. 3(a) shows a pair of the microstrip antennas illuminated by an incident field coming from a point source at \$\vec{r}\_o = (r\_o, \theta, 0)\$. The antennas are linked by a microstrip line of length \$l\$ (from feed point to feed point). Some of the incident field is absorbed by antenna 1, leading to a dominant microstrip mode propagating through the microstrip feed line from antenna 1 to antenna 2. Let \$c\_1\$ be the complex coefficient of this mode at the feed point \$(x\_o, y\_o)\$ of antenna 1 and \$\mathbf{e}\_1\$ be the corresponding tangential modal field. To find \$c\_1\$, the following reciprocity theorem [18] is used:

$$\int_S \mathbf{E}_o \cdot \mathbf{K}_1 ds = \int \mathbf{E}_1 \cdot \mathbf{J}_o dv \quad (1)$$

where \$\mathbf{E}\_o\$ is the tangential field at the cross section \$S\$ of the microstrip line passing through the point \$(x\_o, y\_o)\$, due to the presence of the point source \$\mathbf{J}\_o (= \hat{\theta} I\_o \delta(\vec{r} - \vec{r}\_o))\$. \$\mathbf{K}\_1\$ is a hypothetical surface current distributed at the surface \$S\$, which produces a radiation field \$\mathbf{E}\_1\$ by way of antenna 1. Letting \$\mathbf{K}\_1 = \mathbf{e}\_1\$ and expanding \$\mathbf{E}\_o\$ with the modal fields \$\mathbf{e}\_n, n = 1, 2, \dots\$, of the microstrip line

$$\mathbf{E}_o = \sum_n c_n \mathbf{e}_n \quad (2)$$

(1) becomes

$$c_1 = I_o \mathbf{E}_{1\theta}(\vec{r} = \vec{r}_o) \quad (3)$$

in which the orthonormality property of the modal fields has been incorporated.

The radiation field \$E\_{1\theta}\$ of antenna 1 due to the presence of the surface current \$\mathbf{K}\_1 (= \mathbf{e}\_1)\$ can be obtained from the cavity-mode theory of the microstrip antenna [19]

$$E_{1\theta}(\theta) = \frac{e^{-jk_o r_o}}{r_o} e^{jk_o x_o \sin \theta} G(\theta) \quad (4)$$

with

$$G(\theta) = A_f \cos\left(\frac{k_o a_e}{2} \sin \theta\right) \quad (5)$$

where \$a\_e\$ is the effective length of the microstrip antenna, \$a\_e = a + (h/2)\$, with \$a\$ being the physical antenna length and \$h\$ the thickness of the antenna substrate. \$A\_f\$ is a feed (complex) factor depending on the configuration of the antenna feed.

The microstrip dominant mode excited at antenna 1 propagates through the feed line to antenna 2, causing a reradiation field \$E\_{\theta 2-1}\$ to the source point. The field of the microstrip mode at the feed point \$(-x\_o, y\_o)\$ of antenna 2 is \$c\_1 e^{-jk\_m l} \mathbf{e}\_1\$, which, by the equivalent current principle [18], can be viewed as excited by a surface current

$$\mathbf{K}_2 = \left(\frac{-2}{\eta_m} c_1 e^{-jk_m l}\right) \mathbf{e}_1 = \left(\frac{-2}{\eta_m} c_1 e^{-jk_m l}\right) \mathbf{K}_1$$

at the feed point. (\$k\_m = (2\pi/\lambda\_m)\$ and \$\eta\_m = (\eta\_o/\sqrt{\epsilon\_{re}})\$, with \$\lambda\_m\$ and \$\epsilon\_{re}\$ being the wavelength and the effective relative dielectric constant of the microstrip line, \$\eta\_o\$ the intrinsic impedance of the free-space.) Therefore

$$E_{\theta 2-1} = -\left(\frac{-2}{\eta_m} c_1 e^{-jk_m l}\right) E'_{1\theta} \quad (6)$$

where \$E'\_{1\theta}\$ has the same form as (4) but with \$x\_o\$ substituted by \$-x\_o\$. Note that since antenna 2 has an opposite polarization to antenna 1, a minus sign is added in (6). Casting (3) and (4) into (6), one obtains

$$E_{\theta 2-1} = I_o \left(\frac{e^{-jk_o r_o}}{r_o}\right)^2 \left(\frac{2}{\eta_m}\right) e^{-jk_m l} G^2(\theta). \quad (7)$$

By following the above procedure, it is easy to find that \$E\_{\theta 1-2}\$, i.e., the reradiated field from antenna 1, is exactly equal to \$E\_{\theta 2-1}\$. Thus, the total reradiated field \$E\_{\theta}^r\$ from all the antenna pairs is

$$E_{\theta}^r = I_o \left(\frac{e^{-jk_o r_o}}{r_o}\right) \left(\frac{4}{\eta_m} M\right) e^{-jk_m l} G^2(\theta) \quad (8)$$

where \$M\$ is the number of antenna pairs that equals six in the present design. Note that the phase of \$E\_{\theta}^r\$ depends on the length (\$l\$) of the microstrip feed lines and also that \$E\_{\theta}^r\$ is proportional to the square of the radiation pattern (\$G(\theta)\$) of a single-array element.

To compute the scattered field, PO and the method of equivalent currents (MEC) are used [17]. By the PO method,

the backscattering field from the flat plate to the source point [Fig. 3(b)] is

$$E_{\theta, \text{PO}}^s = I_o \left( \frac{e^{-jk_o r_o}}{r_o} \right)^2 \left( \frac{-k_o^2 \eta_o LW}{8\pi^2} \right) \cdot \left( \frac{\sin(k_o L \sin \theta)}{k_o L \sin \theta} \right) \cos \theta. \quad (9)$$

This expression gives a very accurate result when  $|\theta| < \theta_{\text{null}}$ , with  $\theta_{\text{null}} (= \sin^{-1}(\lambda_o/2L))$  being the angle where the first null of  $E_{\theta, \text{PO}}^s$  appears. As  $|\theta|$  is increased larger than  $\theta_{\text{null}}$ , the field predicted by PO becomes underestimated. A more reliable expression can be obtained by using the MEC, which is an extension of the geometrical theory of diffraction (GTD) for applications in three-dimensional problems [17]

$$E_{\theta, \text{MEC}}^s = I_o \left( \frac{e^{-jk_o r_o}}{r_o} \right)^2 \left( \frac{-k_o^2 \eta_o LW}{8\pi^2} \right) \cdot \left( \frac{\sin(k_o L \sin \theta)}{k_o L \sin \theta} - \frac{\cos(k_o L \sin \theta)}{jk_o L} \right). \quad (10)$$

The total field  $E_{\theta}$  returning from the array reflector to the source point is

$$E_{\theta}(\theta) = E_{\theta}^r(\theta) + E_{\theta}^s(\theta) \quad (11)$$

where

$$E_{\theta}^s(\theta) = \begin{cases} E_{\theta, \text{PO}}^s(\theta), & \text{for } |\theta| < \theta_{\text{null}} \\ E_{\theta, \text{MEC}}^s(\theta), & \text{for } |\theta| > \theta_{\text{null}}. \end{cases} \quad (12)$$

#### IV. CALCULATION AND MEASUREMENT RESULTS

As can be seen from (11) and (8) due to the interference between the reradiated field and the scattered field, the pattern of the total reflected field will change when the length ( $l$ ) of the microstrip lines is varied. To verify this, three array reflectors with the same design parameters but different  $l$ 's, were made and measured to compare with theoretical results. The lengths are 64, 62, and 65 mm, which, respectively, correspond to  $2.948\lambda_m$ ,  $2.856\lambda_m$ , and  $2.994\lambda_m$  at the frequency of 10.025 GHz. Since the currents on the patches are approximated as PO currents in the theory, there may be a difference between the radiation field level from the actual currents and that from these PO currents. Thus, both the amplitude and the phase of the feed factor  $A_f$  in (5) are adjusted to make up for this difference so that a best match between the theoretical and measured patterns for the reflector of  $l = 64$  mm is met. Once  $A_f$  is decided from this structure, it is also used to compute the patterns for reflectors of  $l = 62$  mm and  $l = 65$  mm. Before discussing the following results, it should be noticed that the received power in the calculated and the measured patterns shown below are normalized to, respectively, the calculated and the measured scattered power of the flat plate at the specular direction ( $\theta = 0^\circ$ ).

Fig. 4 depicts the theoretical results for the total, reradiated, and scattered fields of the reflector with  $l = 64$  mm. It is seen that the reradiated field is a slow-varying function of the angle  $\theta$ , which is the principal contribution to the retrodirectivity of the array reflector. On the contrary, both the amplitude and the phase of the scattered field change quickly with the angle,

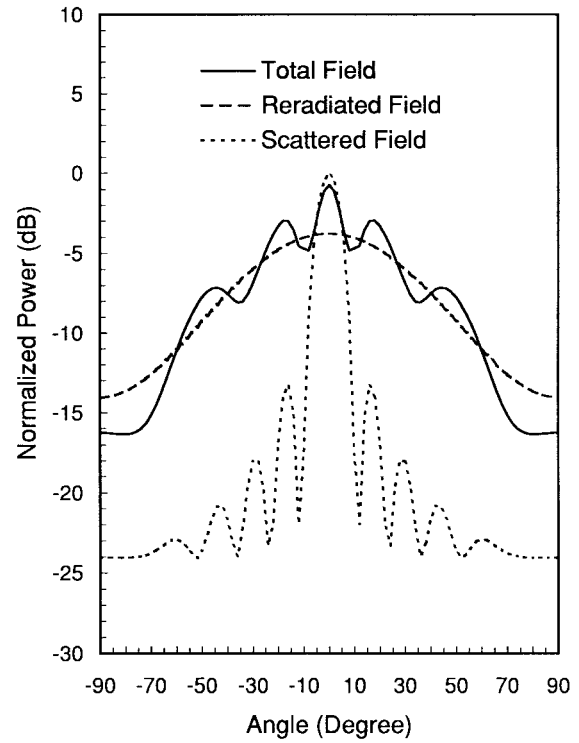


Fig. 4. Theoretical returning-field patterns for a retrodirective reflector of  $l = 64$  mm.

leading to an oscillatory behavior of the total returning field. Since the scattered fields at angles away from the normal of the reflector are much less than the reradiated fields, they can only cause small ripples at these angles. But when the incidence angle is near the reflector normal direction, the scattered field becomes comparable to, if not larger than, the reradiated field. Therefore, different designs of the length of the feed lines, which result in different phases of the reradiated field, may lead to quite distinct total-field patterns near this direction. This will be obvious in the next few illustrations.

Figs. 5–7 show the measured retroreflected-field patterns of the reflectors with  $l = 64$  mm, 62 mm, and 65 mm, respectively. The calculated patterns are also included for comparison. It is seen from Fig. 5 that a smooth pattern is achieved for the design of  $l = 64$  mm. The variation of the reflected field stays within 8 dB in a very wide range of angles (about from  $\theta = -60^\circ$  to  $\theta = +60^\circ$ ). As predicted by the theory, when the length of the feed line is reduced (Fig. 6) or increased (Fig. 7), the measured fields near the reflector normal decrease or increase, respectively. One also observes that at the neighborhoods of  $\theta = \pm \sin^{-1}(\lambda_o/2d) = \pm 56^\circ$ , (where  $d = 18$  mm is the subarray interelement distance,) the measured field levels are larger than the calculated field levels for all the three reflectors. At the angles of  $\theta = \pm 56^\circ$ , the round-trip path difference between the adjacent antennas equals a free-space wavelength and, thus, leads to constructive interference fields scattered from the microstrip antennas. (These scattered fields may be caused by the edge currents induced on the patches and/or by the self-reradiations of the antennas due to the mismatch at the feed points.) Since these coherent fields are not considered in the analysis, the calculated results are thus smaller than the measured ones. Nevertheless,

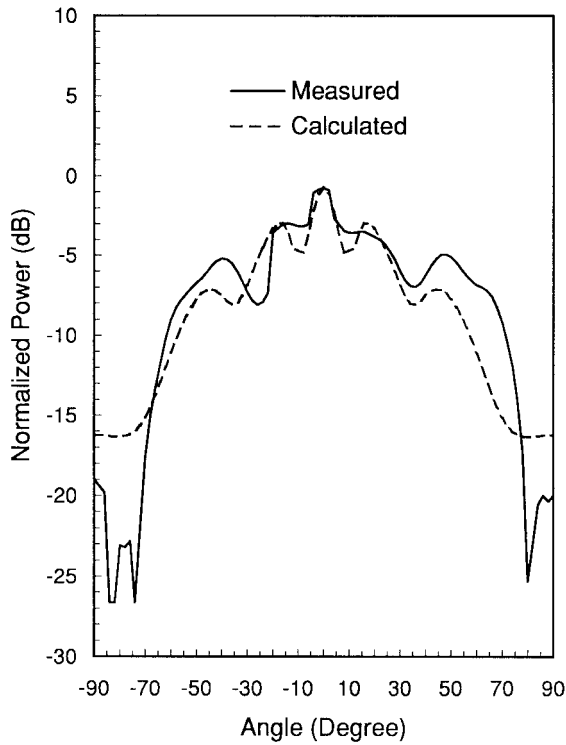


Fig. 5. Comparison between the measured and the calculated returning-field patterns for a retrodirective reflector of  $l = 64$  mm.

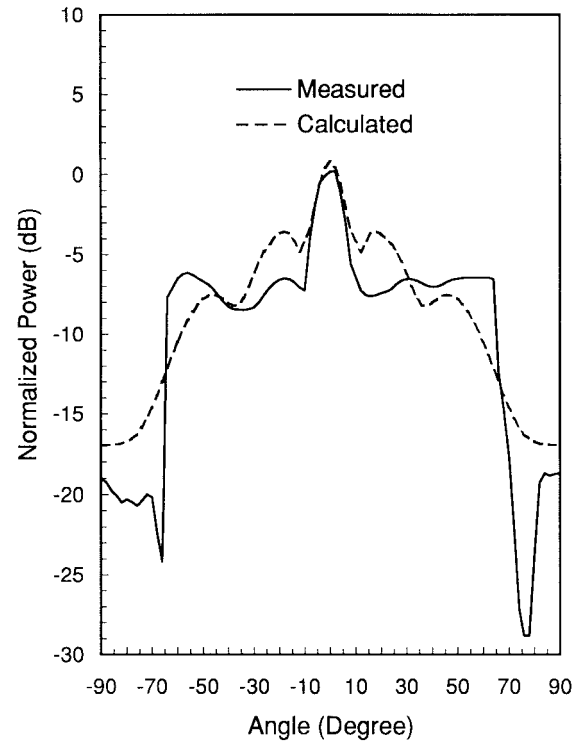


Fig. 7. Comparison between the measured and the calculated returning-field patterns for a retrodirective reflector of  $l = 65$  mm.

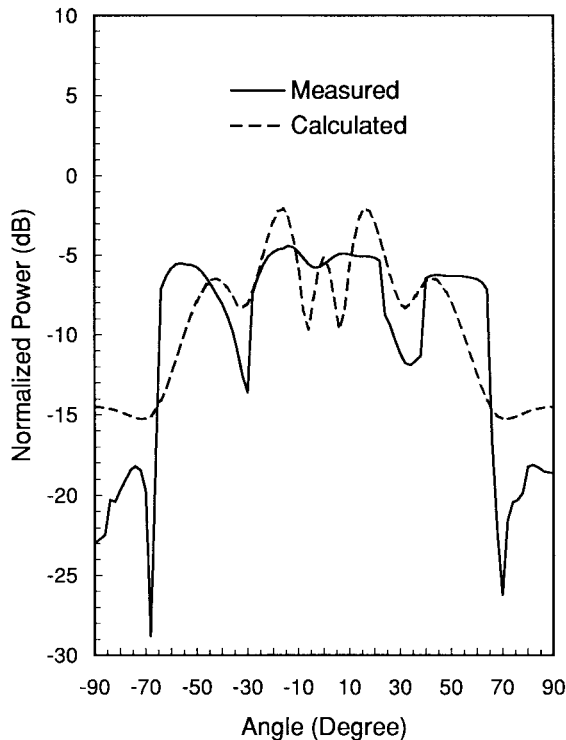


Fig. 6. Comparison between the measured and the calculated returning-field patterns for a retrodirective reflector of  $l = 62$  mm.

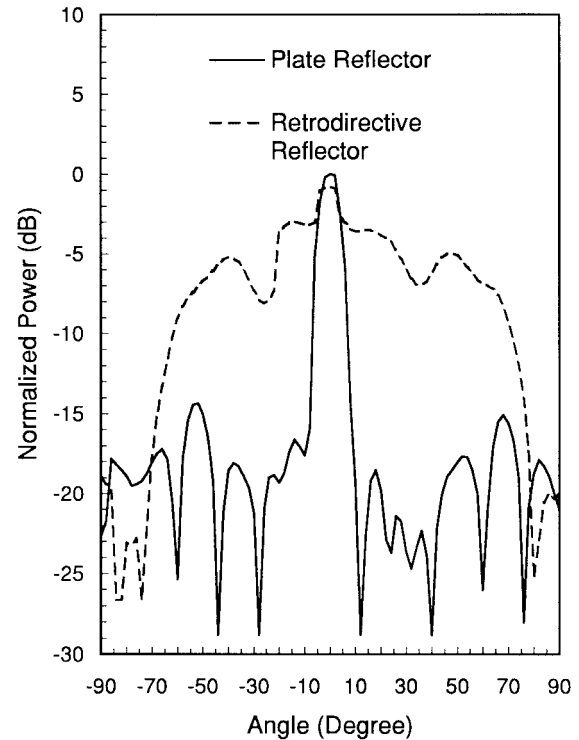


Fig. 8. Measured returning-field patterns for a metal-plate reflector and a retrodirective reflector.

an overview of Figs. 5–7 shows that the present theory is useful in explaining the scattering mechanism of the reflector and in predicting the variation trend of the field patterns due to the change of the feed-line length.

Since the reflector of  $l = 64$  mm has a better performance than the others, it will be used in the following to demonstrate the advantages of the proposed array reflector. Fig. 8 compares the measured patterns of the reflected fields for

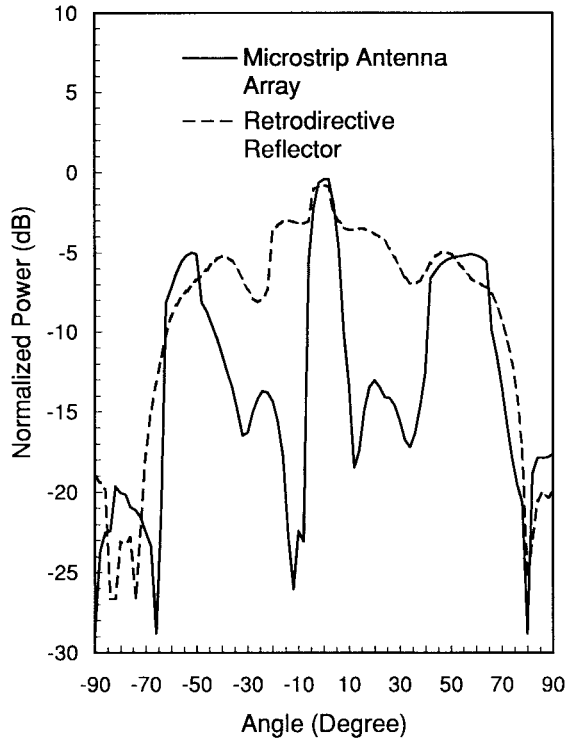


Fig. 9. Measured returning-field patterns for a microstrip antenna array (same elements as the retrodirective reflector but without feed structures) and a retrodirective reflector.

the retrodirective reflector and a plate reflector of the same size. It is seen that the plate reflector only contributes high returning fields in the range between  $\theta = \pm 5^\circ$ . Outside this range, its fields are strongly oscillatory and are much less than those of the retrodirective reflector. Fig. 9 illustrates the backscattering field patterns for a microstrip antenna array and the retrodirective reflector. The geometry of the antenna array is similar to that of the reflector, but without any feed structures. There are three high lobes in the curve of the antenna array, one near the normal direction and the others around  $\theta = \pm 56^\circ$ . The lobe near  $\theta = 0^\circ$  is caused by the specular scattering of the structure, while those around  $\theta = \pm 56^\circ$  are the effects of the self-reradiations and the radiation of edge currents in the array. In between these lobes, the returning fields are much weaker (if not falling to nulls) as compared to those of the retrodirective reflector.

As mentioned earlier, microwave/millimeter-wave switches can be incorporated in the present reflector for the use in communications and remote identifications. One possible design is to place the switches in the middle of the microstrip feed lines. When the switches are in the on-state, guided waves can go through the microstrip lines, leading to high returning fields in a wide range of incidence angles, as has been demonstrated above. But as the switches are in the off-state, the lines are blocked and the waves are reflected back to the incoming antennas, thus destroying the retrodirectivity of the reflector. In this study, gaps with lengths of 2 mm are made in the microstrip lines to simulate a reflector in the off state. The measured pattern of this reflector is shown in Fig. 10, together with that of the on-state reflector for comparison. Owing to a

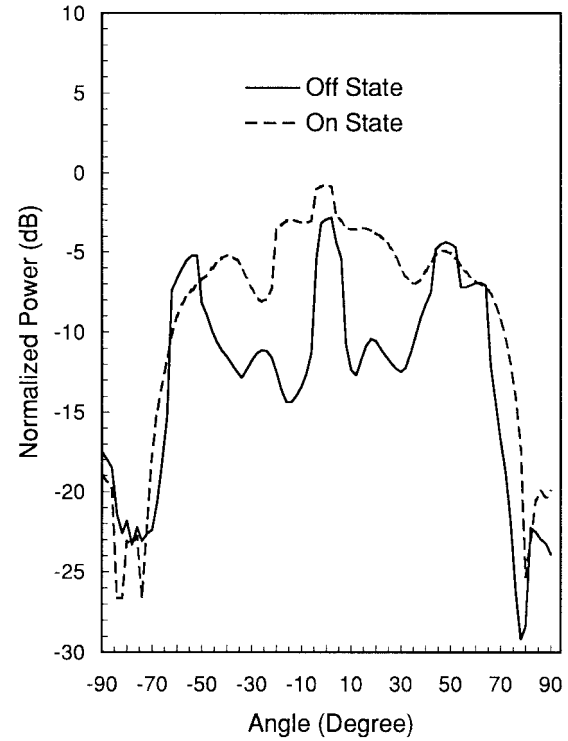


Fig. 10. Measured returning-field patterns for an off-state and an on-state switching retrodirective reflector.

similar reason as for the microstrip antenna array, the off-state reflector has three major lobes. (The distinctions between the patterns of the off-state reflector and the microstrip antenna array are due to the extra microstrip stub attached to each antenna in the off-state reflector, which results in a difference phase of the self-reradiation field.) Only in between these lobes can a larger difference between the off-state and on-state fields exist. In the ranges of  $\theta = -42^\circ$  to  $-7^\circ$  and  $\theta = +7^\circ$  to  $+42^\circ$ , the reflected power of the off-state reflector is about 6 dB (in average) lower than that of the on-state reflector.

Fig. 11 presents the measured H-plane pattern for the reflected fields of the retrodirective reflector ( $l = 64$  mm). Since our structure is only designed for use in the E-plane directions, the H-plane beamwidth is quite narrow as expected. The 3-dB and 10-dB beamwidths are  $11^\circ$  and  $19^\circ$ , respectively.

Figs. 12 and 13 show the reflected-field patterns for the reflector of  $l = 64$  mm at the frequencies of 10.125 and 9.925 GHz, respectively. The return losses at the feed points for these frequencies are both equal to  $-13$  dB, which are 6 dB more than that for the center frequency (10.025 GHz). This return loss results in higher self-reradiation fields due to the reflections at both the feed points of the antennas in the same pair, which, in turn, interfere with the array reradiation field. The patterns with many ripples like those shown in the figures are thus produced. Nevertheless, since the losses are still small for these two frequencies, the ripples do not give large changes on the levels of the patterns.

## V. CONCLUSIONS

In this paper, we have designed and demonstrated the performance of a retrodirective reflector using the aperture-

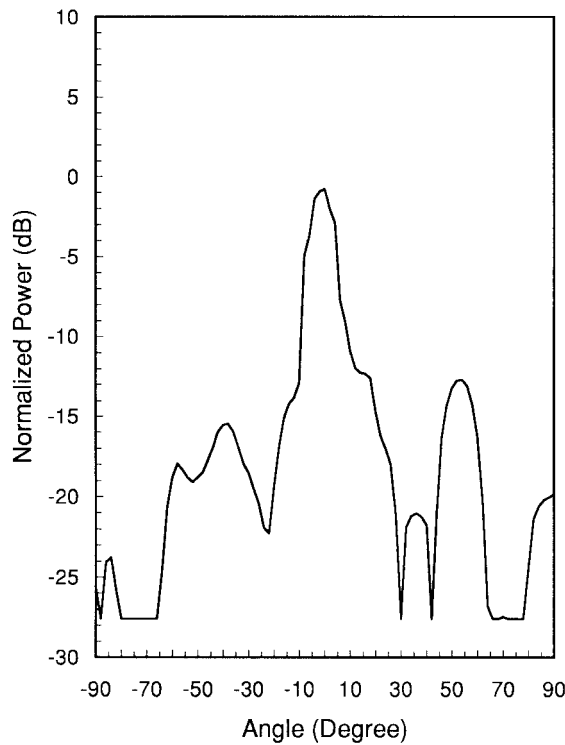


Fig. 11. H-plane returning-field pattern for a retrodirective reflector of  $l = 64$  mm.

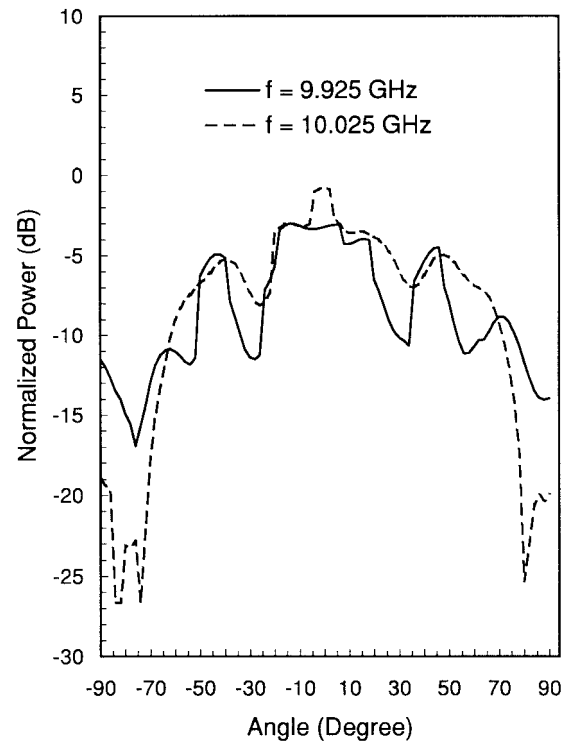


Fig. 13. Measured returning-field patterns for a retrodirective reflector of  $l = 64$  mm at the frequencies of 9.925 and 10.025 GHz.

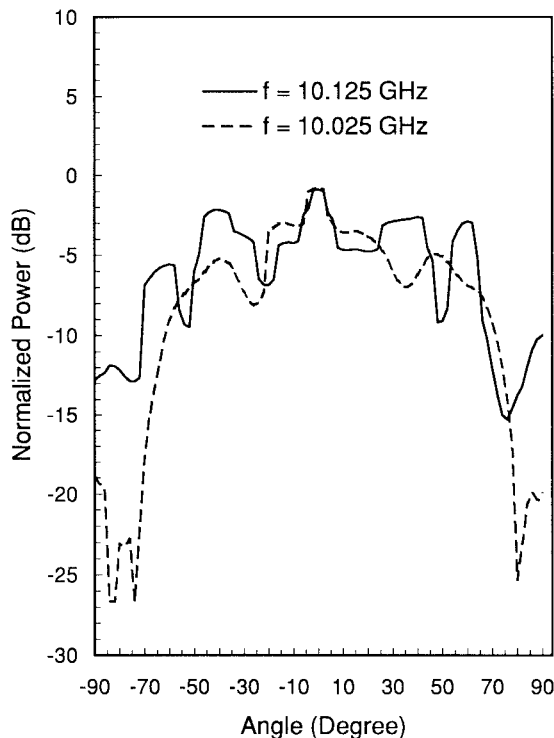


Fig. 12. Measured returning-field patterns for a retrodirective reflector of  $l = 64$  mm at the frequencies of 10.125 and 10.025 GHz.

coupled microstrip antenna array. An approximate theory considering the reradiation and the scattering effects of this array reflector has been introduced, which showed a good agreement with the measurement. According to this theory, the

reradiated fields from the antennas are the primary contribution to the retrodirectivity property of the reflector. The lengths of the microstrip feed lines should be suitably designed so that a well-interfered pattern by the reradiated and scattered fields can be achieved.

The new retrodirective reflector has been compared with a flat-plate reflector of the same size. The returning-field pattern of the former possesses a beamwidth larger than  $120^\circ$ , while that of the latter is only  $10^\circ$ . A comparison has also been made between the present reflector and a microstrip antenna array without a feed structure. Although due to the edge diffraction and self-reradiation effects the microstrip antenna array gives high returning fields at angles away from the specular direction, the fields at other angles are much weaker as compared to the retroreflector. A switching retrodirective reflector together with the field patterns at frequencies off from the designed one was also discussed.

To practically apply the proposed retrodirective configuration in the applications mentioned in the introduction, a larger array reflector may be needed so that stronger echoes can be received. A reflector that not only reradiates the fields in the E-plane but also in the H-plane is also needed. To realize these reflectors, a more complicated routing approach for the feed lines should be considered in the future.

#### ACKNOWLEDGMENT

The authors would like to thank M.-Y. Li and L. Fan for their assistance and suggestions in the measurement. They would also like to thank the reviewers for their careful review and useful suggestions about this paper.

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